

 $\begin{array}{c} \mbox{Application Specific Discretes} \\ \mbox{A.S.D.}^{\rm TM} \end{array}$

MAIN APPLICATIONS

Any telecom equipment submitted to transient overvoltages and lightning strikes such as :

- Analog and ISDN line cards
- PABX

DESCRIPTION

The CLP30-200B1 is designed to protect telecommunication equipment. It provides both a transient overvoltage protection and an overcurrent protection.

The external components (balanced resistors, ring relays contact, ...) needed by the CLP30-200B1 protection concept require very low power rating. This results in a very cost effective protection solution.

FEATURES

- DUAL BIDIRECTIONAL PROTECTION DEVICE.
- HIGH PEAK PULSE CURRENT : IPP = 40A (10/700 μs SURGE) IPP = 30A (10/1000 μs SURGE)
- MAX. VOLTAGE AT SWITCHING-ON : 290V
- MIN. CURRENT AT SWITCHING-OFF : 150mA

BENEFITS

- Voltage and current controlled suppression.
- Surface Mounting with SO8 package.
- Very low power rating of external components on line card : balanced resistors, ring relay, low voltage SLIC protection.

COMPLIES WITH THE FOLLOWING STANDARDS:

CCITT K20	10/700μs 5/310μs	1 kV I _{pp} =25 A
VDE0433	10/700μs 5/310μs	2 kV I _{pp} =40 A (*)
VDE0878	1.2/50μs 1/20μs	1.5 kV I _{pp} =40 A
Bellcore TR-1089-CORE	2/10µs	2.5 kV
FCC Part 68	2/10µs	I _{pp} =75 A (*)
Bellcore TR-NWT-000	10/1000μs 10/1000μs	1 kV I _{pp} =30 A (*)
(*) ''' '' DTO		

(*) with series resistors or PTC.

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OVERVOLTAGE AND OVERCURRENT PROTECTION FOR TELECOM LINE



SCHEMATIC DIAGRAM (Top view)



BLOCK DIAGRAM





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APPLICATION NOTE

1.INTRODUCTION

The aim of this section is to show the behavior of our new telecom line protection device.

Fig.1: Suscriber line protection topology



Figure 1 is a simplified block diagram of a subscriber line protection that is mainly used so far.

This shows two different things :

- A "primary protection" located on the Main Distribution Frame (MDF) eliminates coarsely the high energy environmental disturbances (lightning transients and AC power mains disturbances) for which the CCITT K20 requires a 4kV 10/700 μs test. This can be assumed either by gas-tubes or silicon protection such as the TLPxxM.
- A "secondary protection" located on the line card eliminates finely the remaining transients that have not been totally suppressed by the first stage. The CCITT K20 requires a 1 kV 10/700 µs test. At this stage, the protection is managed by the CLP30-200B1.

The explanations which follow are basically

2. SGS-THOMSON CLP30-200B1 CONCEPT

2.1 Evolution of the SLIC protection

Over the years, the performances of the SLICs considerably increased and therefore the need of the protection has also evolved.

The CLP30-200B1 is especially designed for the protection of this new generation of SLIC. For this, it is based on both overvoltage and overcurrent protection modes.

Fig.2 : Line card protection



The figure 2 summarises the performance of the CLP30-200B1 which basically holds the SLIC inside its correct voltage and current values.



APPLICATION CIRCUIT : CLP30-200B1 in line card

Fig.3 : CLP30-200B1 in line card



Figure above shows the topology of a protected analog subscriber line at the line card side.

- A first stage based on CLP30-200B1 manages the high power issued from the external surges. When used in ringing mode, the CLP30-200B1 operates in voltage mode and provides a symmetrical and bidirectional overvoltage protection above 200 V on both TIP and RING lines. When used in speech mode, the CLP30-200B1 operates in current mode and the activation current of the CLP30-200B1 is adjusted by R_{SENSE}.
- A second stage which is the external voltage reference device defines the firing threshold voltage during the speech mode and also assumes a residual power overvoltage suppression. This stage can be either a fixed or programmable device such as LCP1511D.



2.3 <u>Ringing mode</u>

Fig.4 : Switching by voltage during ringing mode.



In ringing mode (Ring relay in position 2), the only protection device involved is the CLP30-200B1.

In normal conditions, the CLP30-200B1 operates in region 1 of A1 curve, and is idle.

If an overvoltage occurring between TIP (or RING) and GND reaches the internal overvoltage reference (+/- 200V), the CLP30-200B1 acts and the line is short-circuited to GND. At this time the operating point moves to region 2 for positive surges (region 3 for negative surges). Once the surge current disappears, the device returns to its initial state (region 1). For surges occurring between TIP and RING, the CLP30-200B1 acts in the same way. This means that the CLP30-200B1 ensures a tripolar protection.

When used alone, the CLP30-200B1 acts at the internal overvoltage reference level (+/- 200 V). Furthermore, it is possible to adjust this threshold level to a lower voltage by using up to 4 fixed external voltage reference (Vz₁ to Vz₄) (see fig.5).



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Fig.5: Methode to adjust the reference voltage.

2.4 Speech mode

Fig.6 : Switching by current during speech mode.



In speech mode (Ring relay in position 1), the protection is provided by the combination of both CLP30-200B1 and the external voltage reference device (for example LCP1511D).

In normal conditions, the working point of this circuit is located in region 4 of **A2** curve : the CLP30-200B1 is idle.

When a surge occurs on the line, the external voltage reference device clamps at GND or - V_{bat} respectively for positive and negative surges. This generates a current which is detected by R_{SENSE} and causes the protection to act : the line is short-circuited to GND. The operating point moves to region 6 for positive surges or region 5 for negative surges.

Once the surge current falls below the switching-off current I_{SWOFF}, the CLP30-200B1 returns to its initial state (region 4).

Furthermore, the CLP30-200B1 switches when an overvoltage, either positive or negative, occurs either:

- simultaneously on both TIP and RING lines versus GND.
- between TIP and RING.
- on TIP (or RING) versus GND.

The choice of the switching-on current is function of the $\mathsf{R}_{\mathsf{SENSE}}$ resistors.

Fig . 7a and 7b : Switching-on current versus $\mathsf{R}_{\mathsf{SENSE}}$



This current (typically above 150 mA) should not activate the protection device CLP30-200B1.

Therefore the level of activation is to be chosen just below this limit (typically 200mA). This level is adjusted through R_{SENSE}.

Figures 7a and 7b enable the designers to choose the right $R_{\mbox{\scriptsize SENSE}}$ value.

<u>example</u>

The choice of R_{SENSE} = 3 Ω ensures a negative triggering of -280 mA min and -380mA max.

In this case, the positive triggering will be 220mA min and 320mA max.

Thanks to the CLP30-200B1 topology, the surge current in the line is reduced after it.

Because the remaining surge energy is low, the power ratings of R_P , the relay contacts and the external voltage reference device may be kept low. This results in a significant cost reduction for the whole system.

Symbol	Parameter	Value	Unit	
IPP	Line to GND peak pulse current 10/1000 μs (open circuit voltage wave shape 10/ 5/310 μs (open circuit voltage wave shape 10/70	30 40	A	
Ітѕм	Non repetitive surge peak on-state current F = 50 Hz	$\begin{array}{l} t_p = 10 \text{ ms} \\ t_p = 200 \text{ ms} \\ t_p = 1 \text{ s} \end{array}$	8.5 4.5 3.5	A
T _{stg} Tj	Storage temperature range Maximum junction temperature		-40 to +150 150	°C
ΤL	Lead temperature for soldering during 10 s.	260	°C	

ABSOLUTE MAXIMUM RATINGS (R_{SENSE} = 3Ω , T_{amb} = 25° C)

ELECTRICAL CHARACTERISTICS (R_{SENSE} = 3 Ω , and T_{amb} = 25 °C)

Symbol	Parameter	Test condtions	Min	Max	Unit
ILGL	Line to GND leakage current	V_{LG} = 200 V Measured between TIP (or RING) and GND		10	μΑ
V _{LG}	Line to GND operating voltage			200	V
Vswon	Line to GND voltage at SW1 or SW2 switching-on	Measured at 50 Hz between TIPL (or RINGL) and GND, one cycle		290	V
ISWOFF	Line to GND negative current at SW1 or SW2 switching-off	Refer to test circuit fig 9	150		mA
Iswon	Line current at SW1 or SW2 switching-on	Positive surge Negative surge	220 280	320 380	mA
С	Line to GND capacitance	$V_{LG} = 0V$ $V_{OSC} = 200mV_{RMS}$ F = 1MHz		100	pF

THERMAL RESISTANCE

Symbol	Parameter	Value	Unit
R _{th(j-a)}	Junction to ambient	170	°C/W



Fig.8: TEST CIRCUIT FOR ISWOFF PARAMETER: GO- NO GO TEST



Fig. 9: Typical variation of switching-on current (positive or negative) versus RSENSE resistor and junction temperature (see test condition Fig. 11).





- ISWON = I1 when the CLP30-200B1 switches on (I1 is progressively increased using R)

- Both TIP and RING sides of the CLP30-200B1 are checked

 $- RL = 10 \Omega.$



Fig. 10 : Variation of switching-on current versus $\mathsf{R}_{\mathsf{SENSE}}$ at 25 °C.



fig. 12 : Relative variation of switching-off current versus junction temperature (for R_{SENSE} between 3 and 10 Ω).





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fig. 13 : Relative variation of switching-off current versus R_{SENSE} (between 3 and 10 Ω).



Fig. 15 : Relative variation of internal reference voltage versus junction temperature ($I_{LG} = 1mA$).



Fig. 17 : Surge peak current versus overload duration (maximum values).



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Fig. 14 : Relative variation of switching-on voltage versus dV/dt with an external resistor of 3 Ω .



Fig. 16 : Capacitance (TIP/GND) versus applied voltage (typical values).



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ORDER CODE

CLP30-200B1



MARKING

Package	Туре	Marking	
SO8	CLP30-200B1	CLP30	

PACKAGE MECANICAL DATA SO8 plastic



	DIMENSIONS					
REF.	EF. Millimetres Inches			;		
	Min.	Тур.	Max.	Min.	Тур.	Max.
Α			1.75			0.069
a1	0.1		0.25	0.004		0.010
a2			1.65			0.065
b	0.35		0.48	0.014		0.019
b1	0.19		0.25	0.007		0.010
С		0.50			0.020	
c1			45°	(typ)		
D	4.8		5.0	0.189		0.197
E	5.8		6.2	0.228		0.244
е		1.27			0.050	
e3		3.81			0.150	
F	3.8		4.0	0.15		0.157
L	0.4		1.27	0.016		0.050
М			0.6			0.024
S	8° (max)					

Packaging : Product supplied in antistatic tubes or tape and reel

Weight: 0.08g

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