



SBOS445B-JULY 2008-REVISED OCTOBER 2008

# Micro-Power (50μA), Zerø-Drift, Rail-to-Rail Out Instrumentation Amplifier

#### **FEATURES**

• LOW OFFSET VOLTAGE: 25μV (max), G ≥ 100

LOW DRIFT: 0.1µV/°C, G ≥ 100
 LOW NOISE: 50nV/√Hz, G ≥ 100

• HIGH CMRR: 100dB (min), G ≥ 10

• LOW INPUT BIAS CURRENT: 200pA (max)

• SUPPLY RANGE: +1.8V to +5.5V

• INPUT VOLTAGE: (V-) +0.1V to (V+) -0.1V

• OUTPUT RANGE: (V-) +0.05V to (V+) -0.05V

• LOW QUIESCENT CURRENT: 50μA

OPERATING TEMPERATURE: -40°C to +125°C

RFI FILTERED INPUTS

MSOP-8 AND DFN-8 PACKAGES

#### **APPLICATIONS**

- BRIDGE AMPLIFIERS
- ECG AMPLIFIERS
- PRESSURE SENSORS
- MEDICAL INSTRUMENTATION
- PORTABLE INSTRUMENTATION
- WEIGH SCALES
- THERMOCOUPLE AMPLIFIERS
- RTD SENSOR AMPLIFIERS
- DATA ACQUISITION

#### DESCRIPTION

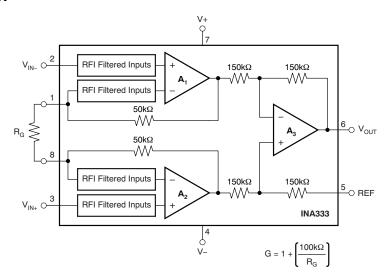
The INA333 is a low-power, precision instrumentation amplifier offering excellent accuracy. The versatile 3-op amp design, small size, and low power make it ideal for a wide range of portable applications.

A single external resistor sets any gain from 1 to 1000. The INA333 is designed to use an industry-standard gain equation:  $G = 1 + (100k\Omega/R_G)$ .

The INA333 provides very low offset voltage  $(25\mu V, G \ge 100)$ , excellent offset voltage drift  $(0.1\mu V/^{\circ}C, G \ge 100)$ , and high common-mode rejection (100dB at  $G \ge 10$ ). It operates with power supplies as low as 1.8V (±0.9V), and quiescent current is only  $50\mu A$ —ideal for battery-operated systems. Using autocalibration techniques to ensure excellent precision over the extended industrial temperature range, the INA333 also offers exceptionally low noise density ( $50nV/\sqrt{Hz}$ ) that extends down to dc.

The INA333 is available in both MSOP-8 and DFN-8 surface-mount packages and is specified over the  $T_A = -40$ °C to +125°C temperature range.

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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### PACKAGE/ORDERING INFORMATION(1)

PRODUCT	PACKAGE-LEAD	PACKAGE DESIGNATOR	PACKAGE MARKING
INIA222	MSOP-8	DGK	1333
INA333	DFN-8	DRG	I333A

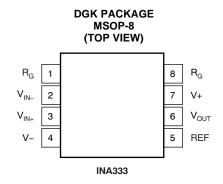
<sup>(1)</sup> For the most current package and ordering information see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

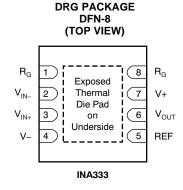
#### **ABSOLUTE MAXIMUM RATINGS(1)**

		INA333	UNIT			
Supply voltage		+7	V			
Analog input vol	Itage range <sup>(2)</sup>	(V-) - 0.3 to (V+) + 0.3	V			
Output short-cire	cuit <sup>(3)</sup>	Continuous	Continuous			
Operating temper	erature range, T <sub>A</sub>	-40 to +150	°C			
Storage tempera	ature range, T <sub>A</sub>	-65 to +150	°C			
Junction temper	rature, T <sub>J</sub>	+150	°C			
	Human body model (HBM)	4000	V			
ESD rating	Charged device model (CDM)	1000	V			
	Machine model (MM)	200	V			

- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.3V beyond the supply rails should be current limited to 10mA or less.
- (3) Short-circuit to ground.

#### **PIN CONFIGURATIONS**





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# ELECTRICAL CHARACTERISTICS: $V_S = +1.8V$ to +5.5V

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$ . At  $T_A = +25^{\circ}C$ ,  $R_L = 10k\Omega$ ,  $V_{REF} = V_S/2$ , and G = 1, unless otherwise noted.

				INA333		
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
INPUT <sup>(1)</sup>						
Offset voltage, RTI <sup>(2)</sup>	V <sub>osi</sub>			±10 ±25/G	±25 ±75/G	μV
vs Temperature					±0.1 ±0.5/G	μ <b>۷/°C</b>
vs Power supply	PSR	$1.8 \text{V} \le \text{V}_{\text{S}} \le 5.5 \text{V}$		±1 ±5/G	±5 ±15/G	$\mu V/V$
Long-term stability				See note (3)		
Turn-on time to specified V <sub>OSI</sub>			See T	ypical charact	eristics	
Impedance						
Differential	$Z_{IN}$			100    3		$G\Omega \parallel pF$
Common-mode	$Z_{IN}$			100    3		$G\Omega \parallel pF$
Common-mode voltage range	$V_{CM}$	$V_O = 0V$	(V-) + 0.1		(V+) - 0.1	V
Common-mode rejection	CMR	DC to 60Hz				
G = 1		$V_{CM} = (V-) + 0.1V$ to $(V+) - 0.1V$	80	90		dB
G = 10		$V_{CM} = (V-) + 0.1V$ to $(V+) - 0.1V$	100	110		dB
G = 100		$V_{CM} = (V-) + 0.1V$ to $(V+) - 0.1V$	100	115		dB
G = 1000		$V_{CM} = (V-) + 0.1V$ to $(V+) - 0.1V$	100	115		dB
INPUT BIAS CURRENT						
Input bias current	I <sub>B</sub>			±70	±200	pA
vs Temperature			See Typi	cal Characteri	stic curve	pA/°C
Input offset current	Ios			±50	±200	pA
vs Temperature			See Typi	cal Characteri	stic curve	pA/°C
INPUT VOLTAGE NOISE						
Input voltage noise	e <sub>NI</sub>	$G = 100, R_S = 0\Omega$				
f = 10Hz				50		$nV/\sqrt{Hz}$
f = 100Hz				50		$nV/\sqrt{Hz}$
f = 1kHz				50		$nV/\sqrt{Hz}$
f = 0.1Hz to 10Hz				1		$\mu V_{PP}$
Input current noise	i <sub>N</sub>					
f = 10Hz				100		fA/√Hz
f = 0.1Hz to 10Hz				2		$pA_{PP}$
GAIN						
Gain equation	G			1 + (100kΩ/R <sub>G</sub>	.)	V/V
Range of gain			1		1000	V/V
Gain error		$V_S = 5.5V$ , $(V-) + 100mV \le V_O \le (V+) - 100mV$				
G = 1				±0.01	±0.1	%
G = 10				±0.05	±0.25	%
G = 100				±0.07	±0.25	%
G = 1000				±0.25	±0.5	%

Total  $V_{OS}$ , Referred-to-input =  $(V_{OSI})$  +  $(V_{OSO}/G)$ . RTI = Referred-to-input.

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<sup>300-</sup>hour life test at +150°C demonstrated randomly distributed variation of approximately 1 $\mu$ V.



# ELECTRICAL CHARACTERISTICS: V<sub>s</sub> = +1.8V to +5.5V (continued)

**Boldface** limits apply over the specified temperature range,  $T_A = -40^{\circ}C$  to  $+125^{\circ}C$ . At  $T_A = +25^{\circ}C$ ,  $R_L = 10k\Omega$ ,  $V_{REF} = V_S/2$ , and G = 1, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
GAIN (continued)							
Gain vs Temperature							
G = 1				±1	±5	ppm/°C	
G > 1 <sup>(4)</sup>				±15	±50	ppm/°C	
Gain nonlinearity		$V_S = 5.5V$ , $(V-) + 100mV \le V_O \le (V+) - 100mV$					
G = 1 to 1000		$R_L = 10k\Omega$		10		ppm	
OUTPUT							
Output voltage swing from rail (5)		$V_S = 5.5V$ , $R_L = 10k\Omega$		See note (5)	50	mV	
Capacitive load drive				500		pF	
Short-circuit current	I <sub>SC</sub>	Continuous to common		-40, +5		mA	
FREQUENCY RESPONSE							
Bandwidth, -3dB							
G = 1				150		kHz	
G = 10				35		kHz	
G = 100				3.5		kHz	
G = 1000				350		Hz	
Slew rate	SR	$V_S = 5V$ , $V_O = 4V$ Step					
G = 1				0.16		V/µs	
G = 100				0.05		V/µs	
Settling time to 0.01%	ts						
G = 1		$V_{STEP} = 4V$		50		μs	
G = 100		$V_{STEP} = 4V$		400		μs	
Settling time to 0.001%	t <sub>S</sub>						
G = 1		V <sub>STEP</sub> = 4V		60		μs	
G = 100		$V_{STEP} = 4V$		500		μs	
Overload recovery		50% overdrive		75		μs	
REFERENCE INPUT							
R <sub>IN</sub>				300		kΩ	
Voltage range			V–		V+	V	
POWER SUPPLY							
Voltage range							
Single			+1.8		+5.5	V	
Dual			±0.9		±2.75	V	
Quiescent current	IQ	$V_{IN} = V_S/2$		50	75	μΑ	
vs Temperature		<del>-</del>			80	μ <b>Α</b>	
TEMPERATURE RANGE							
Specified temperature range			-40		+125	°C	
Operating temperature range			-40		+150	°C	
Thermal resistance	$\theta_{JA}$						
MSOP				100		°C/W	
DFN				65		°C/W	

 <sup>(4)</sup> Does not include effects of external resistor R<sub>G</sub>.
 (5) See Typical Characteristics curve, Output Voltage Swing vs Output Current (Figure 29).



#### TYPICAL CHARACTERISTICS

At  $T_A = +25$ °C,  $V_S = 5$ V,  $R_L = 10$ k $\Omega$ ,  $V_{REF} =$  midsupply, and G = 1, unless otherwise noted.

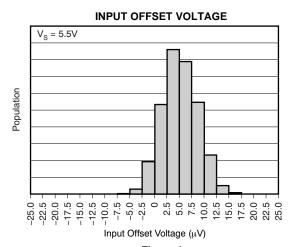
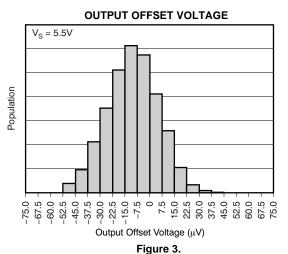
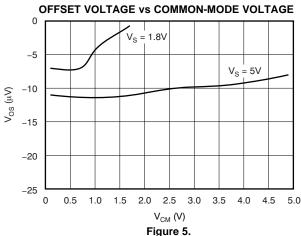


Figure 1.





# INPUT VOLTAGE OFFSET DRIFT (-40°C to +125°C)

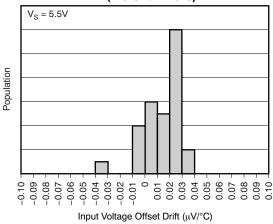


Figure 2.

# OUTPUT VOLTAGE OFFSET DRIFT (-40°C to +125°C)

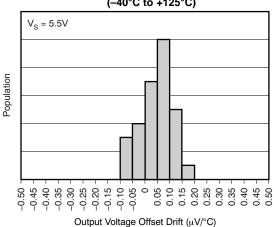


Figure 4.

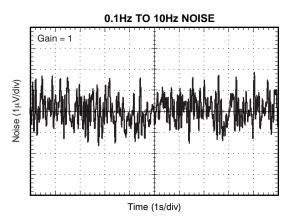
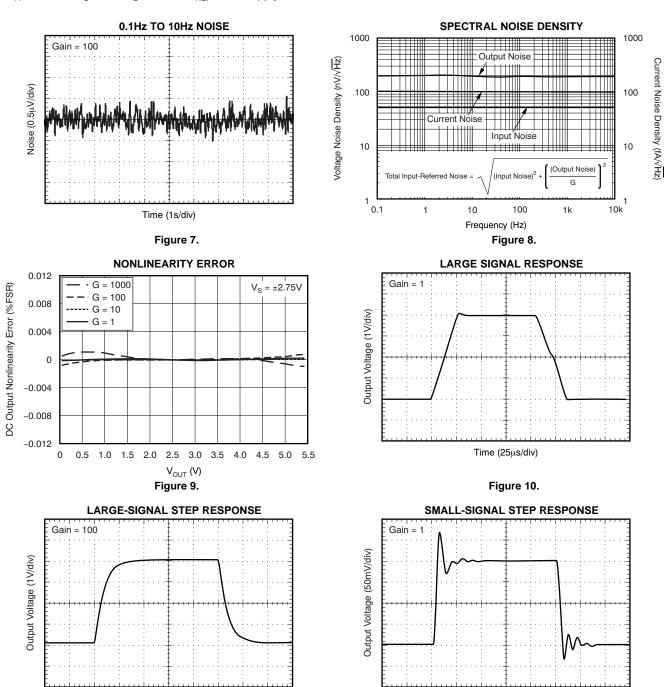


Figure 6.



At  $T_A = +25$ °C,  $V_S = 5$ V,  $R_L = 10$ k $\Omega$ ,  $V_{REF} =$  midsupply, and G = 1, unless otherwise noted.



Time (100µs/div)

Figure 11.

Time (10µs/div)

Figure 12.



At  $T_A$  = +25°C,  $V_S$  = 5V,  $R_L$  = 10k $\Omega$ ,  $V_{REF}$  = midsupply, and G = 1, unless otherwise noted.

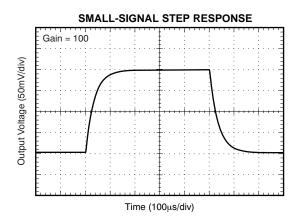


Figure 13.

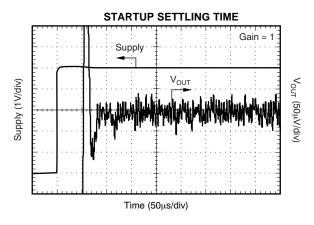
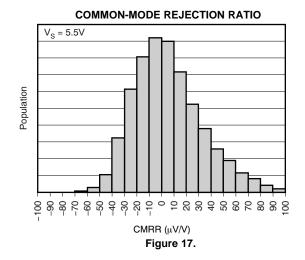


Figure 15.



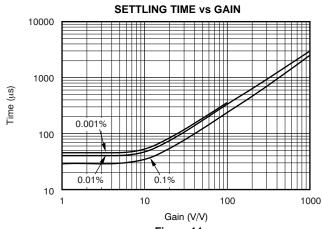
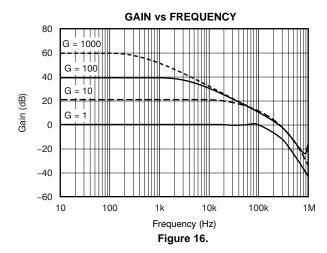


Figure 14.



COMMON-MODE REJECTION RATIO vs TEMPERATURE

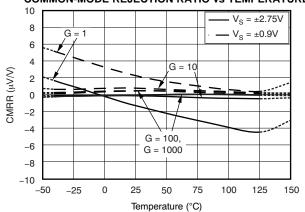
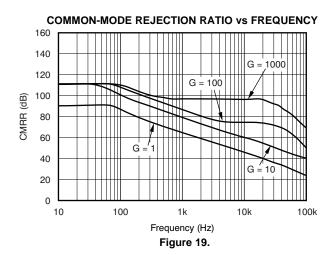


Figure 18.

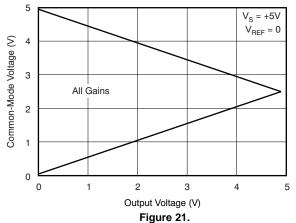
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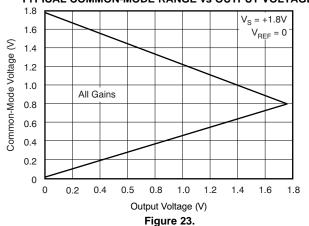
At  $T_A$  = +25°C,  $V_S$  = 5V,  $R_L$  = 10k $\Omega$ ,  $V_{REF}$  = midsupply, and G = 1, unless otherwise noted.



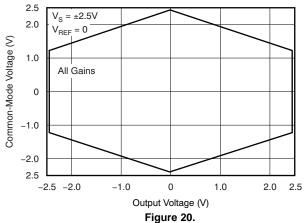
#### TYPICAL COMMON-MODE RANGE vs OUTPUT VOLTAGE



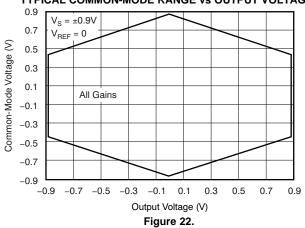
#### TYPICAL COMMON-MODE RANGE vs OUTPUT VOLTAGE



#### TYPICAL COMMON-MODE RANGE vs OUTPUT VOLTAGE



#### TYPICAL COMMON-MODE RANGE vs OUTPUT VOLTAGE



**POSITIVE POWER-SUPPLY REJECTION RATIO** 

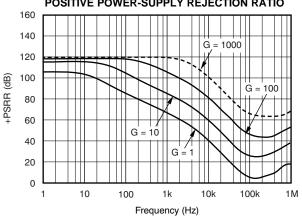
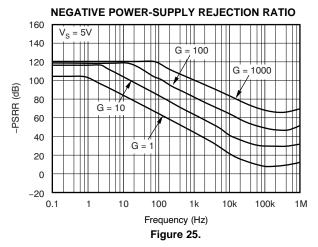
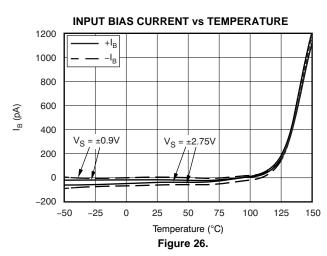


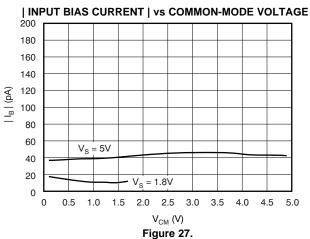
Figure 24.

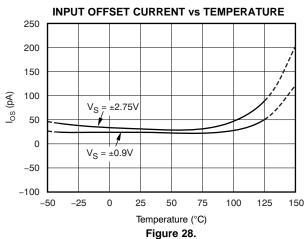


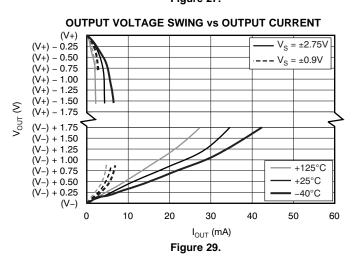
At  $T_A$  = +25°C,  $V_S$  = 5V,  $R_L$  = 10k $\Omega$ ,  $V_{REF}$  = midsupply, and G = 1, unless otherwise noted.











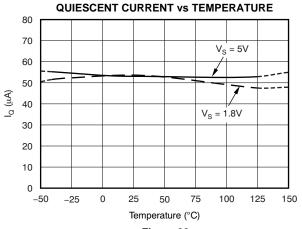


Figure 30.



At  $T_A$  = +25°C,  $V_S$  = 5V,  $R_L$  = 10k $\Omega$ ,  $V_{REF}$  = midsupply, and G = 1, unless otherwise noted.

#### QUIESCENT CURRENT vs COMMON-MODE VOLTAGE 70 V<sub>S</sub> = 5V 60 50 40 V<sub>S</sub> = 1.8V 30 20 10 0 0 1.0 2.0 3.0 4.0 5.0 $V_{CM}$ (V) Figure 31.



#### APPLICATION INFORMATION

Figure 32 shows the basic connections required for operation of the INA333. Good layout practice mandates the use of bypass capacitors placed close to the device pins as shown.

The output of the INA333 is referred to the output reference (REF) terminal, which is normally grounded. This connection must be low-impedance to assure good common-mode rejection. Although  $15\Omega$  or less of stray resistance can be tolerated while maintaining specified CMRR, small stray resistances of tens of ohms in series with the REF pin can cause noticeable degradation in CMRR.

#### **SETTING THE GAIN**

Gain of the INA333 is set by a single external resistor,  $R_{\rm G}$ , connected between pins 1 and 8. The value of  $R_{\rm G}$  is selected according to Equation 1:

$$G = 1 + (100k\Omega/R_G) \tag{1}$$

Table 1 lists several commonly-used gains and resistor values. The  $100k\Omega$  term in Equation 1 comes from the sum of the two internal feedback resistors of  $A_1$  and  $A_2$ . These on-chip resistors are laser trimmed to accurate absolute values. The accuracy and temperature coefficient of these resistors are included in the gain accuracy and drift specifications of the INA333.

The stability and temperature drift of the external gain setting resistor,  $R_{\rm G}$ , also affects gain. The contribution of  $R_{\rm G}$  to gain accuracy and drift can be directly inferred from the gain Equation 1. Low resistor values required for high gain can make wiring resistance important. Sockets add to the wiring resistance and contribute additional gain error (possibly an unstable gain error) in gains of approximately 100 or greater. To ensure stability, avoid parasitic capacitance of more than a few picofarads at the  $R_{\rm G}$  connections. Careful matching of any parasitics on both  $R_{\rm G}$  pins maintains optimal CMRR over frequency.

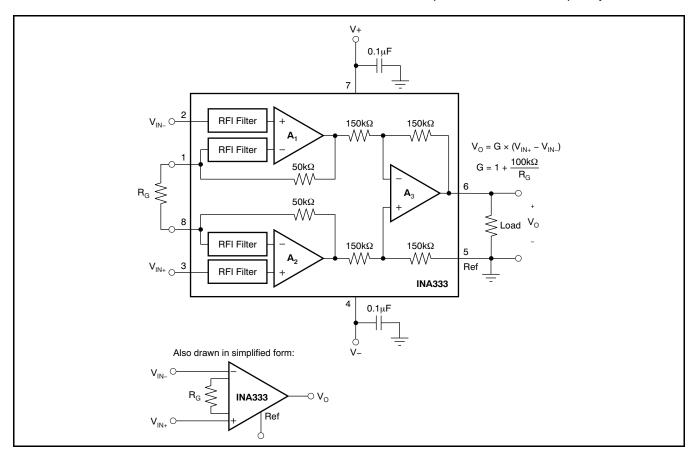


Figure 32. Basic Connections

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Table 1. Commonly-Used Gains and Resistor Values

DESIRED GAIN	R <sub>G</sub> (Ω)	NEAREST 1% R <sub>G</sub> (Ω)
1	NC <sup>(1)</sup>	NC
2	100k	100k
5	25k	24.9k
10	11.1k	11k
20	5.26k	5.23k
50	2.04k	2.05
100	1.01k	1k
200	502.5	499
500	200.4	200
1000	100.1	100

<sup>(1)</sup> NC denotes no connection. When using the SPICE model, the simulation will not converge unless a resistor is connected to the R<sub>G</sub> pins; use a very large resistor value.

#### INTERNAL OFFSET CORRECTION

The INA333 internal op amps use an auto-calibration technique with a time-continuous 350kHz op amp in the signal path. The amplifier is zero-corrected every 8 $\mu$ s using a proprietary technique. Upon power-up, the amplifier requires approximately 100 $\mu$ s to achieve specified  $V_{OS}$  accuracy. This design has no aliasing or flicker noise.

#### **OFFSET TRIMMING**

Most applications require no external offset adjustment; however, if necessary, adjustments can be made by applying a voltage to the REF terminal. Figure 33 shows an optional circuit for trimming the output offset voltage. The voltage applied to REF terminal is summed at the output. The op amp buffer provides low impedance at the REF terminal to preserve good common-mode rejection.

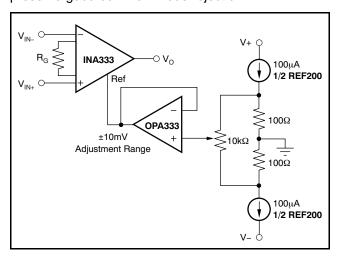


Figure 33. Optional Trimming of Output Offset Voltage

#### NOISE PERFORMANCE

The auto-calibration technique used by the INA333 results in reduced low frequency noise, typically only  $50\text{nV}/\sqrt{\text{Hz}}$ , (G = 100). The spectral noise density can be seen in detail in Figure 8. Low frequency noise of the INA333 is approximately  $1\mu\text{V}_{PP}$  measured from 0.1Hz to 10Hz, (G = 100).

#### INPUT BIAS CURRENT RETURN PATH

The input impedance of the INA333 is extremely high—approximately  $100G\Omega$ . However, a path must be provided for the input bias current of both inputs. This input bias current is typically  $\pm 70$ pA. High input impedance means that this input bias current changes very little with varying input voltage.

Input circuitry must provide a path for this input bias current for proper operation. Figure 34 illustrates various provisions for an input bias current path. Without a bias current path, the inputs will float to a potential that exceeds the common-mode range of the INA333, and the input amplifiers will saturate. If the differential source resistance is low, the bias current return path can be connected to one input (see the thermocouple example in Figure 34). With higher source impedance, using two equal resistors provides a balanced input with possible advantages of lower input offset voltage as a result of bias current and better high-frequency common-mode rejection.



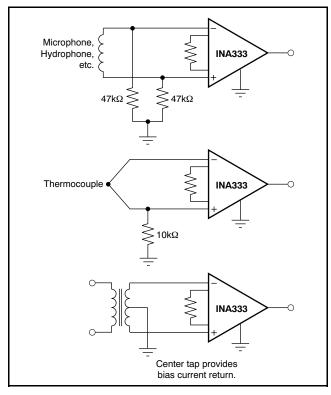


Figure 34. Providing an Input Common-Mode Current Path

#### INPUT COMMON-MODE RANGE

The linear input voltage range of the input circuitry of the INA333 is from approximately 0.1V below the positive supply voltage to 0.1V above the negative supply. As a differential input voltage causes the output voltage to increase, however, the linear input range is limited by the output voltage swing of amplifiers A<sub>1</sub> and A<sub>2</sub>. Thus, the linear common-mode input range is related to the output voltage of the complete amplifier. This behavior also depends on supply voltage—see Typical Characteristic curves Typical Common-Mode Range vs Output Voltage (Figure 20 to Figure 23).

Input overload conditions can produce an output voltage that appears normal. For example, if an input overload condition drives both input amplifiers to the respective positive output swing limit, the difference voltage measured by the output amplifier is near zero. The output of the INA333 is near 0V even though both inputs are overloaded.

#### **OPERATING VOLTAGE**

The INA333 operates over a power-supply range of +1.8V to +5.5V (±0.9V to ±2.75V). Supply voltages higher than +7V (absolute maximum) can permanently damage the device. Parameters that vary over supply voltage or temperature are shown in the Typical Characteristics section of this data sheet.

#### LOW VOLTAGE OPERATION

The INA333 can be operated on power supplies as low as ±0.9V. Most parameters vary only slightly throughout this supply voltage range—see the Typical Characteristics section. Operation at very low supply voltage requires careful attention to assure that the input voltages remain within the linear range. Voltage swing requirements of internal nodes limit the input common-mode range with low power-supply voltage. The **Typical** Characteristic curves **Typical** Common-Mode Range vs Output Voltage (Figure 20 to Figure 23) show the range of linear operation for various supply voltages and gains.

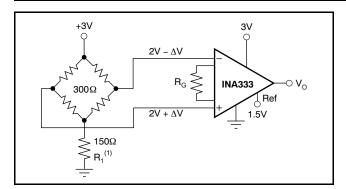
#### SINGLE-SUPPLY OPERATION

The INA333 can be used on single power supplies of +1.8V to +5.5V. Figure 35 illustrates a basic single-supply circuit. The output REF terminal is connected to mid-supply. Zero differential input voltage demands an output voltage of mid-supply. Actual output voltage swing is limited to approximately 50mV above ground, when the load is referred to ground as shown. The typical characteristic curve *Output Voltage Swing vs Output Current* (Figure 29) shows how the output voltage swing varies with output current.

With single-supply operation,  $V_{\text{IN+}}$  and  $V_{\text{IN-}}$  must both be 0.1V above ground for linear operation. For instance, the inverting input cannot be connected to ground to measure a voltage connected to the noninverting input.

To illustrate the issues affecting low voltage operation, consider the circuit in Figure 35. It shows the INA333 operating from a single 3V supply. A resistor in series with the low side of the bridge assures that the bridge output voltage is within the common-mode range of the amplifier inputs.





(1) R<sub>1</sub> creates proper common-mode voltage, only for low-voltage operation—see the *Single-Supply Operation* section.

Figure 35. Single-Supply Bridge Amplifier

#### INPUT PROTECTION

The input terminals of the INA333 are protected with internal diodes connected to the power-supply rails. These diodes clamp the applied signal to prevent it from damaging the input circuitry. If the input signal voltage can exceed the power supplies by more than 0.3V, the input signal current should be limited to less than 10mA to protect the internal clamp diodes. This current limiting can generally be done with a series input resistor. Some signal sources are inherently current-limited and do not require limiting resistors.

#### **GENERAL LAYOUT GUIDELINES**

Attention to good layout practices is always recommended. Keep traces short and, when possible, use a printed circuit board (PCB) ground plane with surface-mount components placed as close to the device pins as possible. Place a  $0.1\mu F$  bypass capacitor closely across the supply pins. These guidelines should be applied throughout the analog circuit to improve performance and provide benefits such as reducing the electromagnetic-interference (EMI) susceptibility.

Instrumentation amplifiers vary in the susceptibility to radio-frequency interference (RFI). RFI can generally be identified as a variation in offset voltage or dc signal levels with changes in the interfering RF signal. The INA333 has been specifically designed to minimize susceptibility to RFI by incorporating passive RC filters with an 8MHz corner frequency at the  $V_{\rm IN+}$  and  $V_{\rm IN-}$  inputs. As a result, the INA333 demonstrates remarkably low sensitivity compared to previous generation devices. Strong RF fields may continue to cause varying offset levels, however, and may require additional shielding.

#### APPLICATION IDEAS

Additional application ideas are shown in Figure 36 to Figure 39.

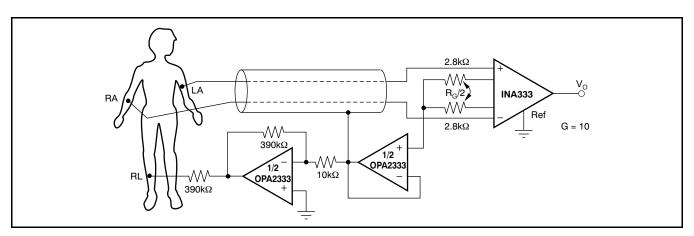


Figure 36. ECG Amplifier With Right-Leg Drive

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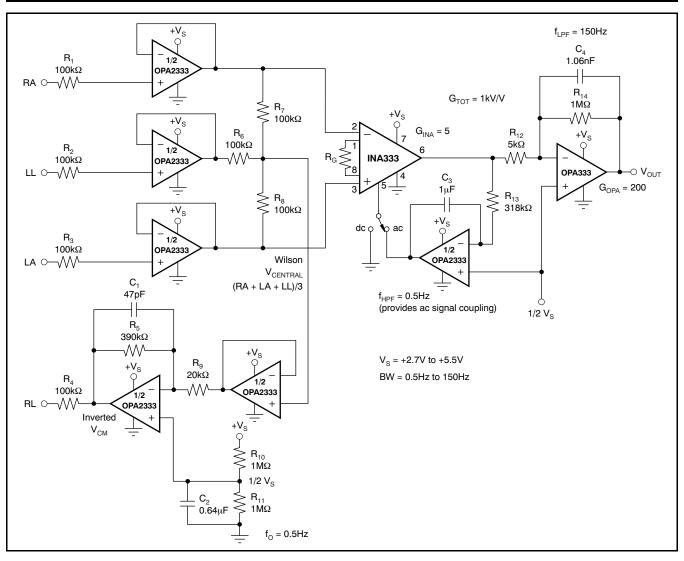


Figure 37. Single-Supply, Very Low Power, ECG Circuit

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#### TINA-TI (FREE DOWNLOAD SOFTWARE)

# Using TINA-TI SPICE-Based Analog Simulation Program with the INA333

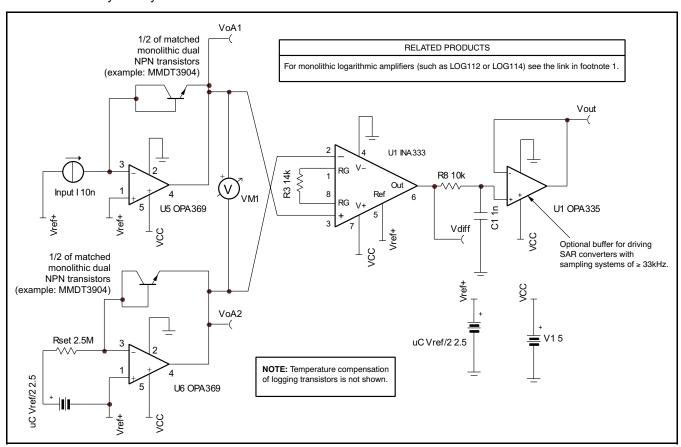
TINA is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI is a free, fully functional version of the TINA software, preloaded with a library of macromodels in addition to a range of both passive and active models. It provides all the conventional dc, transient, and frequency domain analysis of SPICE as well as additional design capabilities.

Available as a free download from the Analog eLab Design Center, TINA-TI offers extensive post-processing capability that allows users to format results in a variety of ways.

Virtual instruments offer users the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

Figure 38 and Figure 39 show example TINA-TI circuits for the INA333 that can be used to develop, modify, and assess the circuit design for specific applications. Links to download these simulation files are given below.

**NOTE:** these files require that either the TINA software (from DesignSoft) or TINA-TI software be installed. Download the free TINA-TI software from the TINA-TI folder.

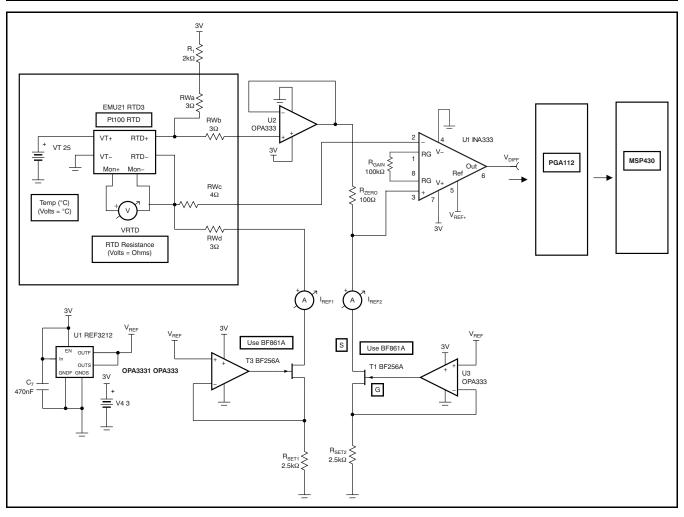


(1) The following link launches the TI logarithmic amplifiers web page: Logarithmic Amplifier Products Home Page

Figure 38. Low-Power Log Function Circuit for Portable Battery-Powered Systems (Example Glucose Meter)

To download a compressed file that contains the TINA-TI simulation file for this circuit, click the following link: Log Circuit.





RWa, RWb, RWc, and RWd simulate wire resistance. These resistors are included to show the four-wire sense technique immunity to line mismatches. This method assumes the use of a four-wire RTD.

Figure 39. Four-Wire, 3V Conditioner for a PT100 RTD With Programmable Gain Acquisition System

To download a compressed file that contains the TINA-TI simulation file for this circuit, click the following link: PT100 RTD.





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#### **PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/ Ball Finish	MSL Peak Temp <sup>(3)</sup>	Samples (Requires Login)
INA333AIDGKR	ACTIVE	VSSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
INA333AIDGKRG4	ACTIVE	VSSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
INA333AIDGKT	ACTIVE	VSSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
INA333AIDGKTG4	ACTIVE	VSSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
INA333AIDRGR	ACTIVE	SON	DRG	8	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
INA333AIDRGT	ACTIVE	SON	DRG	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	

<sup>&</sup>lt;sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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### PACKAGE OPTION ADDENDUM

16-Aug-2012

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

#### **OTHER QUALIFIED VERSIONS OF INA333:**

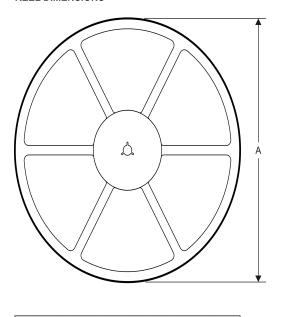
NOTE: Qualified Version Definitions:

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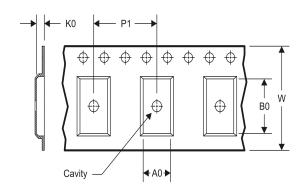
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#### TAPE AND REEL INFORMATION

#### **REEL DIMENSIONS**



#### **TAPE DIMENSIONS**



A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

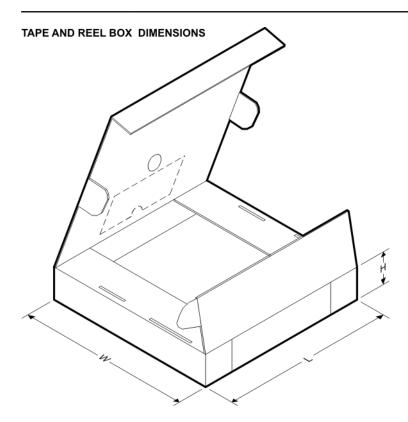
#### TAPE AND REEL INFORMATION

\*All dimensions are nominal

All dimensions are nominal	All differsions are normal											
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
INA333AIDGKR	VSSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
INA333AIDGKT	VSSOP	DGK	8	250	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
INA333AIDRGR	SON	DRG	8	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
INA333AIDRGT	SON	DRG	8	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2

**PACKAGE MATERIALS INFORMATION** 

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\*All dimensions are nominal

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Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
INA333AIDGKR	VSSOP	DGK	8	2500	366.0	364.0	50.0
INA333AIDGKT	VSSOP	DGK	8	250	366.0	364.0	50.0
INA333AIDRGR	SON	DRG	8	3000	367.0	367.0	35.0
INA333AIDRGT	SON	DRG	8	250	210.0	185.0	35.0

# DGK (S-PDSO-G8)

# PLASTIC SMALL-OUTLINE PACKAGE



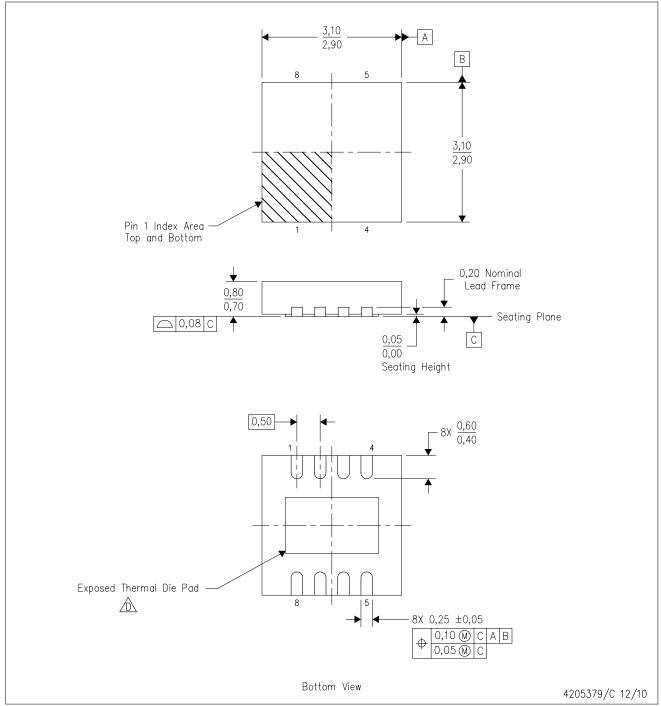
NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
- E. Falls within JEDEC MO-187 variation AA, except interlead flash.



# DRG (S-PWSON-N8)

# PLASTIC SMALL OUTLINE NO-LEAD



- NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M—1994.
  - B. This drawing is subject to change without notice.
  - C. SON (Small Outline No-Lead) package configuration.
  - The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.
  - E. JEDEC MO-229 package registration pending.



# DRG (S-PWSON-N8)

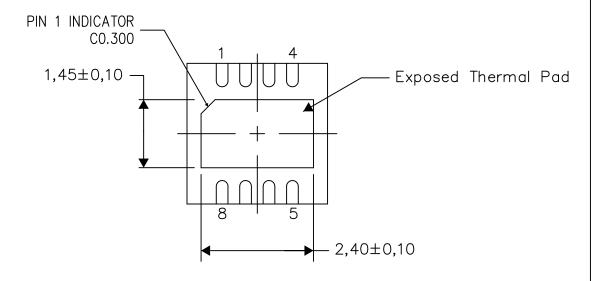
#### PLASTIC SMALL OUTLINE NO-LEAD

#### THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No—Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



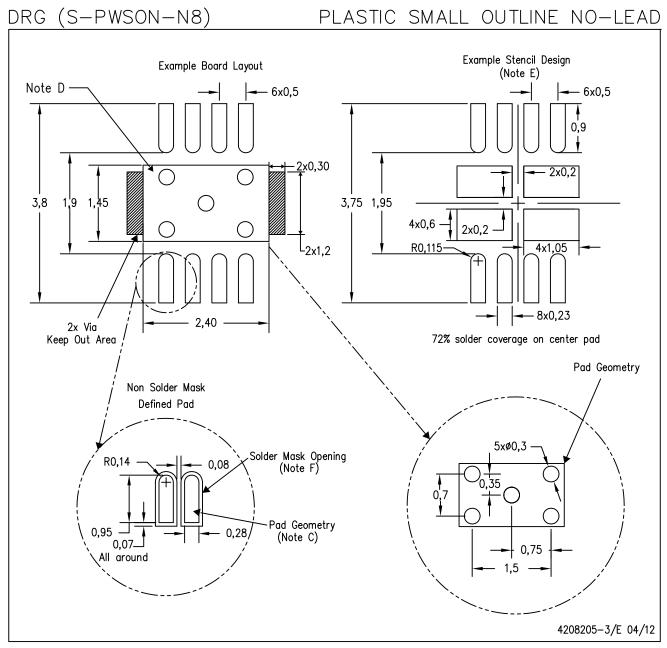
Bottom View

Exposed Thermal Pad Dimensions

4206881-3/G 04/12

NOTE: All linear dimensions are in millimeters





NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-SM-782 is recommended for alternate designs.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Application Note, Quad Flat—Pack Packages, Texas Instruments Literature No. SLUA271, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC 7525 for stencil design considerations.
- F. Customers should contact their board fabrication site for minimum solder mask web tolerances between signal pads.



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