

PRELIMINARY

LH4104/LH4104C Fast Settling High Current Operational Amplifier

General Description

The LH4104 is a fast settling high current Bi-Fet op amp designed for applications that require a fast settling time of 500 ns to 0.01% and 100 mA continuous output current. The high output current eliminates the need for a buffer to provide the additional current drive not available in most operational amplifiers. The operational amplifier also features a gain bandwidth product of 18 MHz and a slew rate of $40V/\mu s$.

Designed for use with minimum external circuitry, the LH4104 provides internal compensation for unity gain stability as well as internal supply bypass capacitors. These features minimize the circuit's sensitivity to external layout conditions.

Features

- 500 ns settling time to 0.01% for a 10V step
- 100 mA continuous output current
- 18 MHz gain bandwidth product
- Internal supply bypassing
- Unity gain stable

Applications

- Cable Drivers
- High Speed Ramp Generators
- DAC Output Amplifiers
- Fast Buffers
- Sample and Holds
- Fast Integrators

Schematic Diagram



Absolute Maximum Ratings

If Military/Aerospace specified devices are required, contact the National Semiconductor Sales Office/ Distributors for availability and specifications. Supply Voltage, V_S \pm 18V Steady State Output Current, I_o 100 mA Power Dissipation at, P_D $T_A = 25^{\circ}$ C, derate linearly at 100°C/W 2.5W $T_C = 25^{\circ}$ C, derate linearly at 50°C/W 1.5W

\pm 30V but $\leq \pm$ 2V _s
\pm 18V but $\leq \pm V_s$
-55°C to +125°C
-25°C to +85°C
-65°C to +150°C
150°C
300°C

DC Electrical Characteristics $V_S = \pm 15V$, $T_A = 25^{\circ}C$ unless otherwise noted (Note 1)

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	Parameter	Conditions		LH41040	Units	
Symbol			Тур	Tested Limit (Note 2)	Design Limit (Note 3)	(Max Unless Otherwise Stated)
V _{OS}	Input Offset Voltage	$R_{S} = 50\Omega$	2	5	10	mV
V _{OS} /∆T	Offset Voltage Drift	$R_{S} = 50\Omega$	20			μV/°C
۱ _B	Input Bias Current	$T_{i} = 25^{\circ}C$, (Note 4) $V_{CM} = 0V$	200	600		рА
					250	nA
los	Input Offset Current	$T_{j} = 25^{\circ}C, V_{CM} = 0V$	20	400		pА
					200	nA
R _{IN}	Input Resistance	$T_j = 25^{\circ}C$	1011			Ω
AVOL	Large Signal Voltage Gain	$R_L = 100\Omega$	106	87		dB (Min)
		$R_L = 1 k\Omega$	106	87	80	
Vo	Output Voltage Swing	$R_L = 100\Omega$ (Note 5)		±10		
		$R_L = 1 k\Omega$	±13	±10	± 10	V (Min)
V _{CM}	Input Common Mode Range		±12	±11	± 10	V (Min)
CMRR	Common Mode Rejection Ratio	$V_{IN} = -11V \text{ to } + 11V$	100	80	70	dB (Min)
PSRR	Power Supply Rejection Ratio	$V_{CC} = \pm 10V \text{ to } \pm 15V$	100	80	70	dB (Min)
IS	Supply Current		20	25		mA

AC Electrical Characteristics $V_{CC} = \pm 15V$, $T_A = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Conditions	LH4104C			Units
			Тур	Tested Limit (Note 2)	Design Limit (Note 3)	(Max Unless Otherwise Stated)
ts	Settling Time to 0.01%	$A_V = -1, V_{IN} = -5V \text{ to } +5V, R_L = 100\Omega$	500	800		ns
SR	Slew Rate	$V_{IN} = -10V \text{ to } + 10V, R_L = 100\Omega$	40		32	V/µs(min)
GBW	Gain Bandwidth Product		18			MHz
tr	Small Signal Rise Time	$A_V = 1, R_L = 100\Omega$	10		20	ns

Symbol	Parameter	Conditions		LH4104		Units
			Тур	Tested Limit (Note 2)	Design Limit (Note 3)	(Max Unless Otherwise Stated)
V _{OS}	Input Offset Voltage	$R_{S} = 50\Omega$	2	10		mV
V _{OS} /∆T	Offset Voltage Drift	$R_{S} = 50\Omega$	20			μV/°C
I _B	Input Bias Current	$T_j = 25^{\circ}C$, (Note 4) $V_{CM} = 0V$	200	600		pА
				350		nA
los	Input Offset Current	$T_{j} = 25^{\circ}C, V_{CM} = 0V$	20	400		pА
				250		nA
R _{IN}	Input Resistance	T _j = 25°C	1011			Ω
A _{VOL}	Large Signal Voltage Gain	$R_L = 100\Omega$	106	87	-	dB (Min)
		$R_L = 1 k\Omega$	106	87		
				80		
Vo	Output Voltage Swing	$R_L = 100\Omega$ (Note 5)		±10		
		$R_L = 1 k\Omega$	±13	± 10		V (Min)
V _{CM}	Input Common Mode Range		±12	± 10		V (Min)
CMRR	Common Mode Rejection Ratio	V _{IN} -11V to +11V	V _{IN} -11V to +11V 100 80			
					70	
PSRR	Power Supply Rejection Ratio	$V_{CC} = \pm 10V \text{ to } \pm 15V$	100	80		dB (Min)
				70		
ls	Supply Current		20	25		mA

AC Electrical Characteristics $V_{CC} = \pm 15V$, $T_A = 25^{\circ}C$ unless otherwise noted

	Parameter	Conditions		LH4104	Units	
Symbol			Тур	Tested Limit (Note 2)	Design Limit (Note 3)	(Max Unless Otherwise Stated)
ts	Settling Time to 0.01%	$A_V = -1, V_{IN} = -5V \text{ to } +5V, R_L = 100\Omega$	500	800		ns
SR	Slew Rate	$V_{\rm IN} = -10V$ to $+10V$, $R_{\rm L} = 100\Omega$	40		32	V/µs(min)
GBW	Gain Bandwidth Product		18			MHz
tr	Small Signal Rise Time	$A_V = 1, R_L = 100\Omega$	10		20	ns

Note 1: Boldface limits are guaranteed over full temperature range. Operating ambient temperature range of LH4104C is -25°C to +85°C, and LH4104 is -55°C to +125°C.

Note 2: Tested limits are guaranteed and 100% production tested.

Note 3: Design limits are guaranteed (but not production tested).

Note 4: Specifications is at 25°C junction temperature due to requirements of high speed automatic testing. Actual values at operating temperature will exceed value at $T_j = 25°C$.

Note 5: The output swing is limited by the maximum output current of ± 100 mA when R_L = 100 Ω .

Note 6: When the LH4104 is operated at elevated temperture (such as 125°C), some form of heat sinking or forced air cooling is required. The quiescent power with V_{CC} of ±15V is 750 mW, whereas the package can only handle 500 mW without a heatsink at 125°C.

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Applications Information

POWER SUPPLY BYPASSING

The LH4104 will perform well in most circuit boards even without external supply bypassing; however it is recommended that some bulk bypassing be provided to maintain optimum settling time. A 0.1 µF disc ceramic capacitor and 1 µF tantalum capacitor on each supply is recommended. Place the bypass capacitors close to the amplifiers supply pins.

COMPENSATION

To minimize the effects of input capacitance at the LH4104's inverting input and any additional layout capacitance, an external compensation capacitor must be used. The compensation capacitor (C1) used in Figure 2 (Test Circuit Section) is typically 66 pF. The optimum value for the compensation capacitor depends on the application circuit and the board layout.

INPUT BIAS CURRENT

The input devices are JFETs, and will normally have input bias (I_R) currents in the tens of picoamps. However, these

currents vary with temperature and input voltage range. IB will normally double with each 11°C rise in junction temperature.

125 150

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LAYOUT PRECAUTIONS

Grounding and circuit layout are extremely important in preserving the settling time of the LH4104. It is important to use single point ground returns for inputs, loads, and feedback components and to keep the returns short. Compensation components should be located close to the appropriate pins to minimize stray reactances. Keep the system's digital signals (or any other signals with fast rise times) separated from the amplifier. If such signals are too close to the amplifier, they can couple capacitively to the amplifier's inputs, resulting in undesirable signals at the output.

PRESERVING AND VERIFYING THE LH4104'S FAST SETTLING TIME

To realize optimum settling performance in circuits using the LH4104, both the design and layout must be meticulous. Application note AN-428, "Preserving and Verifying the

Applications Information (Continued)

LF400's Fast Settling Time", explains the required design and measurement techniques. Although this application note was written for the LF400, it suggests good guidelines and is directly applicable to the LH4104. Only the sections covering supply bypassing and output load limitations should be ignored. This is because the LH4104 has internal bypassing capacitors and substantially greater output drive current than the LF400. The suggested circuits require only small and straightforward modifications; even the printed circuit board layout can be easily modified to accept the footprint of the LH4104 without impacting setting time.

PROTECTION SCHEMES FOR THE LH4104

The LH4104 has similar input characteristics of National Semiconductor's BI-FET™ family of operational amplifiers. As such, designing with this part requires that several precautions are observed which are uncharacteristic of other op amps. Application Note AN-447 covers these caveats in greater detail for the whole product family. (The LH4104's input stage shares its topology with the LF400.)

NEVER LEAVE AN INPUT UNATTENDED!

If an input to the LH4104 is left open circuited (or connected to an analog multiplexer in a high impedance state), the input bias current will be drawn from the very small parasitic input capacitance (<10 pF). This capacitor will rapidly charge up to the power supply rail at a rate of dv/dt =IBIAS/CIN. Since the LH4104 is a capable of large output currents and has no internal current limiting, it will easily be destroyed by excessive power dissipation if such an input condition exists while driving a low impedance load (e.g. **50Ω)**.

To avoid this condition in circuits where the LH4104 is buffering the FET switch of an analog multiplexer, one must connect a resistor between the input and ground to provide a bias current path. This will invariably degrade the effective input impedance of the device, so a large resistor is desirable.

For example, selecting a 1 M Ω resistor will result in a harmless 25 mV output signal during the "deselected" state (for the worst case bias current of 25 nA). Increasing this resistor will increase the output signal for the deselected" state; decreasing it will reduce this signal while degrading the input impedance. Depending on the user's circuit specifications, a compromise must be selected. This resistor will not introduce an increase in the effective offset voltage during the "selected" state because the input is driven by a low impedance source.

POWER SUPPLY SEQUENCING

Adding the clamp diodes shown in Figure 1 not only protects the inputs from transients when the circuit is operating, but protects them as power is being applied to the circuit. Because the parasitic transistor apears when the input voltage is less than the negative supply, applying the positive supply or input voltage before the negative supply is applied can cause this problem. For this reason, it is always recommended that the negative supply be turned on first, if the supplies can be turned on independently.

Also, even if the input stage is well protected with clamp diodes and current limiting, the inputs should not be allowed to be heavily unbalanced (for example, one input at ground and the other at the rail) for extended periods of time (for example, many hours). The long-term effects of an unbalanced differential pair are increased offset voltage and offset current.



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FIGURE 1. Clamping Inputs of Op Amp

VOS ADJUSTMENT

Offset voltage can be nulled using a 56K resistor and a 25K potentiometer connected to pins 3 and 7 as shown in Figure 3. Bypassing the V_{OS} adjust pins with 0.1 μ F capacitors will help to avoid noise pickup. When not used for offset adjustment, pins 3 and 7 can often be left open, but to minimize the possibility of noise pickup the unused VOS trim pins should be connected to ground or V-.

Test Circuit for Pulse Response



FIGURE 2

