National Semiconductor Corporation

# LM2005 20-Watt Automotive Power Amplifier

**Typical Application** 

#### **General Description**

The LM2005 is a dual high power amplifier, designed to deliver optimum performance and reliability for automotive applications. High current capability (3.5A) enables the device to deliver 10W/channel into  $2\Omega$  (LM2005T-S), or 20W bridged monaural (LM2005T-M) into  $4\Omega$ , with low distortion.

### Features

- Wide supply range (8V-18V)
- Externally programmable gain

**Connection Diagram** 

- With or without bootstrap
- Low distortion
- Low noise

- High peak current capability
- P<sub>O</sub>=20W bridge
- High voltage protection
- AC and DC output short circuit protection to ground or across load
- Thermal protection
- Inductive load protection
- Accidental open ground protection
- Immunity to 40V power supply transients
- 3°C/W device dissipation
- Pin for pin compatible with TDA2005

**Plastic Package** TAB CONNECTED TO PIN 6 ROOTSTRAP 1 OUTPUT 1 10 + VS BOOTSTRAP 2 GND INPUT +2 NPUT -2 BYPASS NPUT - 1 INPUT +1 TOP VIEW TL/H/5129-1

Order Number LM2005T-S or LM2005T-M See NS Package Number T11A



TL/H/5129-2

FIGURE 1. 20W Bridge Amplifier Application and Test Circuit

## LM2005T-M and LM2005T-S Absolute Maximum Ratings

If Military/Aerospace specified devices are required, contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Operating Supply Voltage	187
DC Supply Voltage (Note 1)	28V
Peak Supply Voltage (50 ms)	40V

Output Current	
Repetitive (Note 2)	3.5A
Non-Repetitive	4.5A
Power Dissipation	30W
Operating Temperature	-40°C to +85°C
Storage Temperature	-60°C to +150°C
Lead Temp. (Soldering, 10 seconds)	260°C

## LM2005T-M

**Electrical Characteristics** Refer to the **bridge** application circuit, *Figure 1*,  $T_{amb} = 25^{\circ}C$ ,  $A_V = 50 \text{ dB}$ ,  $R_{th (heatsink)} = 4^{\circ}C/W$ , unless otherwise specified

Parameter	Test C	conditions	Min	Тур	Max	Units
Supply Voltage			8		18	v
Output Offset Voltage (Note 3) (between Pin 8 and 10)	$V_{S} = 14.4V$ $V_{S} = 13.2V$			±20	± 150 ± 150	mV mV
Total Quiescent Drain Current Includes Current in Feedback Resistors	$V_{S} = 14.4V$ $V_{S} = 13.2V$	$R_{L} = 4\Omega$ $R_{L} = 3.2\Omega$		75 70	150 160	mA mA
Output Power	d = 10% V <sub>S</sub> = 14.4V V <sub>S</sub> = 13.2V	$f = 1 \text{ kHz}$ $R_{L} = 4\Omega$ $R_{L} = 3.2\Omega$ $R_{L} = 3.2\Omega$	18 20 17	20 22 19		w w w
THD	$f = 1 \text{ kHz}$ $V_S = 14.4V$ $P_O = 50 \text{ mW to}$ $V_S = 13.2V$ $P_O = 50 \text{ mW to}$	15W R <sub>L</sub> = 3.2 $\Omega$			1	%
Input Sensitivity	f = 1  kHz $P_0 = 2W$ $P_0 = 2W$	$R_L = 4\Omega$ $R_L = 3.2\Omega$		9 8		mV mV
Input Resistance	f = 1  kHz	-	70			kΩ
Low Frequency Roll Off (-3 dB)	$R_L = 3.2\Omega$				40	Hz
High Frequency Roll Off (-3 dB)	$R_L = 3.2\Omega$		20			kHz
Closed Loop Voltage Gain	f = 1 kHz	-	45	50		dB
Total Input Noise Voltage	$R_g = 10 k\Omega$ (Ne	ote 4)		3	10	μV
Supply Voltage Rejection	$R_g = 10 k\Omega$ $C_4 = 10 \mu F$	f <sub>ripple</sub> = 100 Hz V <sub>ripple</sub> = 0.5V	45	55		dB
Efficiency	$V_{S} = 14.4V$ $P_{O} = 20W$ $P_{O} = 22W$ $V_{S} = 13.2V$ $P_{O} = 19W$	$R_L = 3.2\Omega$		60 60 58		%
Output Voltage with One Side of the Speaker Shorted to Ground	$V_{S} = 14.4V$ $V_{S} = 13.2V$	$R_{L} = 4\Omega$ $R_{L} = 3.2V$			2	v

Note 1: Internal voltage limit. Shuts down above 20V.

Note 2: Internal current limit.

Note 3: For LM2005T-M only.

Note 4: Bandwidth filter: 22 Hz to 22 kHz.

# LM2005

# LM2005T-S

**Electrical Characteristics** Refer to the stereo application circuit, *Figure 2*,  $T_{amb} = 25^{\circ}C$ ,  $G_{v} = 50 \text{ dB}$ , Rth (heaterisk) = 4°C/W, unless otherwise specified

Parameter	Test	Conditions	Min	Тур	Max	Units
Supply Voltage			8		18	V
Quiescent Output Voltage	$V_{\rm S} = 14.4 V$		6.6	7.2	7.8	v
	V <u>S</u> = 13.2V		6	6.6	7.2	v
Total Quiescent Drain Current	V <sub>S</sub> = 14.4V			65	120	mA
Includes Current in Feedback Resistors	$V_{\rm S} = 13.2V$			62	120	mA
Output Power	f = 1  kHz	d = 10%				
(Each Channel)	$V_{S} = 14.4V$	$R_{L} = 4\Omega$ $R_{I} = 3.2\Omega$	6 7	6.5 8		w w
		$R_{L} = 3.2\Omega$ $R_{L} = 2\Omega$	9	10		w
		$R_L = 1.6\Omega$	10	11		Ŵ
	$V_{\rm S} = 13.2V$	$R_L = 3.2\Omega$	6	6.5		w
		$R_L = 1.6\Omega$	9	10		w
	V <sub>S</sub> = 16V	$R_L = 2\Omega$		12		w
THD	f = 1 kHz					
(Each Channel)	$V_{\rm S} = 14.4V$	-		0.0		%
	$P_O = 50 \text{ mW to}$ $V_S = 14.4 \text{V}$	$R_{I} = 2\Omega$		0.2	1	70
	$P_0 = 50 \text{ mW to}$	-		0.3	1	%
	$V_{\rm S} = 13.2V$	$R_{L} = 3.2\Omega$				
	$P_O = 50 \text{ mW to}$	3W		0.2	1	%
	V <sub>S</sub> = 13.2V	$R_L = 1.6\Omega$				
	$P_0 = 40 \text{ mW to}$	6W		0.3	1	%
Cross Talk	$V_{\rm S} = 14.4V$	f = 1 kHz	40	60		dB
(Note 5)	$R_{L} = 4\Omega$ $V_{O} = 4 V_{rms}$					<u> </u>
	$R_{\rm q} = 5  \mathrm{k}\Omega$	f = 10 kHz		40		dB
Input Saturation Voltage			300			 mV
Input Sensitivity	f = 1 kHz	P <sub>O</sub> = 1W				
		$R_L = 4\Omega$		6		
		$R_L = 3.2\Omega$	_	5.5		mV
Input Resistance	f = 1 kHz	Non-Inverting Input	70	200		kΩ
		Inverting Input		10		kΩ
Low Frequency Roll Off ( $-3  dB$ )	$R_L = 2\Omega$				50	Hz
High Frequency Roll Off (-3 dB)	$R_L = 2\Omega$		15			kHz
Voltage Gain (Open Loop)	f = 1 kHz			90		dB
Voltage Gain (Closed Loop)	f = 1 kHz		48	50	51	dB
Closed Loop Gain Matching				0.5		dB
Total Input Noise Voltage	$R_g = 10 k\Omega$ (No	ote 6)		1.5	5	μV
Supply Voltage Rejection	$R_g = 10 k\Omega$	f <sub>ripple</sub> =100 Hz				
	$C_3 = 10 \mu\text{F}$	V <sub>ripple</sub> =0.5V	35	45		dB
Efficiency	$V_{S} = 14.4V$	f = 1 kHz	[			
	$R_{L} = 4\Omega$	$P_{O} = 6.5W$		70		%
	$R_{L} = 2\Omega$	$P_0 = 10W$		60		%
	$V_{\rm S} = 13.2V$	f = 1  kHz				
	$R_L = 3.2\Omega$	$P_0 = 6.5W$		70		%
	$R_L = 1.6\Omega$	P <sub>O</sub> = 10W	L	60	I	%

Note 6: Bandwidth filter: 22 Hz to 22 kHz.



1-209

LM2005

Components	Omponents (Figure 2) Comments	Components	Comments
1. R1, R2 R5, R4	Sets voltage gain,	5. C4, C5	Bootstrap capacitors, used to increase drive to output stage.
	$A_V \cong 1 + \frac{R'}{R1}$ for one channel, B'	6. C3	Improves power supply rejection. Increasing C3 increases turn-on delay (approximately 2 ms per $\mu$ F).
	$A_V = 1 + \frac{R'}{R5}$ for the other. Where R' is the equivalent resistance	7. C2, C6	Inverting input DC decouple. Low frequency pole:
	of R2 in parallel with an internal 10k resistor:		$F_{L}2 = \frac{1}{2\pi Z(\text{inverting})C2}$
	$R' = \frac{10k \bullet R2}{R2 + 10k}$		Z (inverting) $\approx$ 10 k $\Omega$ .
	If R2 ≪ 10k, then	8. C <sub>C</sub>	Output coupling capacitor. Isolates pins 10 and 8 from load. Low
	$A_V \cong 1 + \frac{R2}{R1}$		frequency pole;
2. R3	Adjusts output symmetry for maximum		$F_{L}3 = \frac{1}{2\pi R_{L}C_{C}}$
	power output.	9. C <sub>S</sub>	Power supply filtering.
3. R <sub>O</sub> , C <sub>O</sub>	Works to stabilize internal output stage. Necessary for stability. C <sub>O</sub>		
	should be ceramic disc or equivalently good high frequency capacitor.		
4. C1, C9	Input coupling capacitor. Low frequency pole set by		
	$F_{L}1 = \frac{1}{2\pi Z \text{ (non-inverting) C1}}$ Decreasing capacitor value will also		
	increase noise.		
Typical Ap			
Typical Ar	increase noise.		ν <sub>s</sub> 
Typical Ar	increase noise.	0.1 µ <sup>F</sup> Ţ 100 µ <sup>F</sup> ¶ 100 µ <sup>F</sup> ¶	$\begin{array}{c} & \downarrow \\ & \downarrow \\$
Typical Ar	increase noise. <b>Splications</b> (Continued) $10 \mu F$ $120k$ $10 \mu F$ $120k$ $10 \mu F$ $120k$ $10 \mu F$ $120k$ $10 \mu F$ $100 \mu F$ $100 \mu F$ $100 \mu F$	0.1 µ <sup>F</sup> Ţ 100 µ <sup>F</sup> ¶ 100 µ <sup>F</sup> ¶	$\begin{array}{c} \begin{array}{c} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & $
Typical Ap	increase noise. <b>Oplications</b> (Continued) $10 \mu F$ $120k$ $10 \mu F$ $120k$ $10 \mu F$ $120k$ $11 \mu F$ $1/2$ $11 \mu F$ $100 \mu F$ $1/2$ $10 \mu F$		$\begin{array}{c} \begin{array}{c} \begin{array}{c} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \begin{array}{c} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \begin{array}{c} \\ \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \\ \end{array} \\ $
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LM2005

#### **Application Hints**

The high current capability of the LM2005 allows it to continuously endure either AC or DC short circuit of the output with a maximum supply voltage of 16V. This will protect the loudspeaker in a bridge mode, when a DC short of the output occurs on one side of the speaker. The device will prevent the speaker from destruction by reducing the DC across the load (bridge mode) to typically less than 2  $V_{\rm DC}(V_{\rm S}{=}14.4V,~R_{\rm L}{=}4\Omega),$  by an internal current pullback method.

The LM2005 can withstand a constant 28 V<sub>DC</sub> on the supply with no damage (maximum operating voltage is 18V). The device is also protected from load dump or dangerous transients up to 40V for 50 ms (every 1000 ms) on the supply with no damage.

Protection diodes protect the device driving inductive loads, during which the load can generate voltages greater than supply or less than ground levels. The protection diodes will clamp these transients to a safe  $\mathsf{V}_{\mathsf{BE}}$  above and below the rails.

The bridge configuration in *Figure 3* is designed for applications requiring minimal printed circuit board area and maximum cost effectiveness. The circuit will function with the elimination of bootstrap components R3, C4 and C5 (refer to *Figure 1*). This will result in less output power by decreasing output voltage swing to the load. By using internal feedback resistors (typically 10 k $\Omega$ ), feedback components R2, R3 and C2 (*Figure 1*) may be omitted where closed loop voltage gain accuracy is not critical. The net result is a stable, cost effective circuit that will satisfy many application needs.



Ay = 41.5 dB @ 1 kHz

FIGURE 3. Minimal Component Application Circuit

Component Side (Scale 2:1)

