19-4022; Rev 0; 4/91

# **High-Side Power Supplies**

#### **General Description**

The MAX622/MAX623 high-side power supplies, using a regulated charge-pump, generate a regulated output voltage 11V greater than the input supply voltage to power high-side switching and control circuits. The MAX622/MAX623 allow low-resistance N-Channel MOSFETs (FETs) to be used in circuits that normally require costly, less efficient P-Channel FETs and PNP transistors. The high-side output also eliminates the need for logic FETs in +5V and other low-voltage switching circuits.

A +3.5V to +16.5V input supply range and a typical quiescent current of only  $70\mu A$  make the MAX622/MAX623 ideal for a wide range of line- and battery-powered switching and control applications where efficiency is crucial. Also provided is a logic-level Power-Ready Output (PR) to indicate when the high-side voltage reaches the proper level.

The MAX622 comes in 8-pin DIP and SO packages and requires three inexpensive external capacitors. The MAX623 is supplied in 16-pin DIPs only, but contains internal capacitors and requires no external components.

#### Applications

- High-Side Power Control with N-Channel FETs Low-Dropout Voltage Regulators Power Switching from Low Supply Voltages H-Switches Stepper Motor Drivers Battery-Load Management
- Portable Computers

#### **Typical Operating Circuit**





MAX622/MAX623

- ♦ +3.5V to +16.5V Operating Supply Voltage Range
- ♦ Output Voltage Regulated to V<sub>CC</sub> + 11V (Typ)
- ♦ 70µA Typ Quiescent Current
- Power-Ready Output

#### **Ordering Information**

TEMP. RANGE	PIN-PACKAGE
0 C to +70 C	8 Plastic DIP
0 C to +70 C	8 SO
0 C to +70 C	Dice*
-40 C to +85 C	8 Plastic DIP
-40 C to +85 C	8 SO
0 C to +70 C	16 Plastic DIP
-40 C to +85 C	16 Plastic DIP
	0 C to +70 C 0 C to +70 C 0 C to +70 C -40 C to +85 C -40 C to +85 C 0 C to +70 C

\*Contact factory for dice specifications.

#### **Pin Configurations**



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#### Call toll free 1-800-998-8800 for free samples or literature.

## **ELECTRICAL CHARACTERISTICS (MAX623)**

PARAMETER	SYMBOL	CONDITIONS	MIN	ТҮР	MAX	UNITS
Supply Voltage	Vcc		3.5		16.5	V
		IOUT = 0. VCC = 3.5V	11.5	12.5	16.5	1
		IOUT = 0. VCC = 4.5V	14.5	15.5	17.5	· V
Fals Olds Maltana (Nisto 4)	Marin	IOUT = 0, VCC = 16.5V	26.5	27.5	29.5	
High-Side Voltage (Noto 1)	I Vout	$I_{OUT} = 50 \mu A. V_{CC} = 3.5 V$	8.5	10.5	16.5	
		$I_{OUT} = 250 \mu A. V_{CC} = 5V$	15		18	
		$I_{OUT} = 500 \mu A. V_{CC} = 16.5 V$	26.5		29.5	
Power-Ready Threshold	PRT	IOUT = 0 (Note 3)	12	13.5	14.5	V
Power-Ready Output High	PROH	$I_{SOURCE} = 100 \mu A$	3.8	4.3	5	V
Power-Ready Output Low	PROL	ISINK = 1mA			0.4	V
Dutput Voltage Ripple	VR	lout = 500μA (Note 4)		100		mV
Switching Frequency	Fo			90		кHz
Quiescent Supply Current	bly Current IQ	$I_{OUI} = 0, V_{CC} = 5V.$ $T_A = +25 \text{ C}$		70	500	
		IOUT = 0, VCC = 16.5V, TA = +25 C		70	350	μA

Note 1: High-Side Voltage measured with respect to ground. Note 2: For V<sub>CC</sub> > +13V on the MAX622, use C1 = C2 =  $0.01\mu$ F. Note 3: Power-Ready Threshold is the voltage with respect to ground at V<sub>OUT</sub> when PR switches high (PR - V<sub>CC</sub>). Note 4: Output Voltage Ripple on the MAX623 may be reduced by adding an external 10 $\mu$ F reservoir capacitor.

			Pin Description	1
MAX622 8-PIN	MAX623 16-PIN	NAME	FUNCTION	1
1		C1+	Positive terminal to primary charge-pump capacitor.	
	1-5. 11-13. 15. 16	I.C.	Internal Connection. Make no connection to this pin.	
2		C2-	Negative terminal to secondary charge-pump capacitor.	
3	6	PR	Power-Ready Output. High when $V_{OUT}$ is $\geq V_{CC} + 8.5V$ with respect to GND.	'
4	7,8	GND	Ground	
5	9, 10	Vout	High-Side Voltage Out	
6		C2+	Positive terminal to secondary charge-pump capacitor.	
7		C1-	Negative terminal to primary charge-pump capacitor.	
8	14	Vcc	Input Supply	

## **Bin Description**

## **ELECTRICAL CHARACTERISTICS (MAX623)**

PARAMETER	SYMBOL	CONDITIONS	MIN	ТҮР	MAX	UNITS
Supply Voltage	Vcc		3.5		16.5	V
		IOUT = 0. VCC = 3.5V	11.5	12.5	16.5	
		$I_{OUT} = 0. V_{CC} = 4.5 V$	14.5	15.5	17.5	
Eab Olda Valtaga (Nata 1)		$I_{OUT} = 0, V_{CC} = 16.5V$	26.5	27.5	29.5	V
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		$I_{OUT} = 250 \mu A. V_{CC} = 5 V$	15		18	
		$I_{OUT} = 500 \mu A. V_{CC} = 16.5 V$	26.5		29.5	
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Power-Ready Output Low	PROL	ISINK = 1mA			0.4	V
Output Voltage Ripple	VR	Ι <sub>ΟUT</sub> = 500μΑ (Note 4)		100		mV
Switching Frequency	Fo			90		кHz
Quiescent Supply Current		$I_{OUI} = 0, V_{CC} = 5V.$ $T_A = +25 C$		70	500	
	IQ	IOUT = 0, VCC = 16.5V. TA = +25 C		70	350	μA

Note 1: High-Side Voltage measured with respect to ground. Note 2: For V<sub>CC</sub> > +13V on the MAX622, use C1 = C2 =  $0.01 \mu$ F. Note 3: Power-Ready Threshold is the voltage with respect to ground at V<sub>OU1</sub> when PR switches high (PR - V<sub>CC</sub>). Note 4: Output Voltage Ripple on the MAX623 may be reduced by adding an external 10 $\mu$ F reservoir capacitor.

			Pin Description
MAX622 8-PIN	MAX623 16-PIN	NAME	FUNCTION
1		C1+	Positive terminal to primary charge-pump capacitor.
	1-5. 11-13, 15. 16	I.C.	Internal Connection. Make no connection to this pin.
2		C2-	Negative terminal to secondary charge-pump capacitor.
3	6	PR	Power-Ready Output. High when $V_{OUT}$ is $\geq V_{CC} + 8.5V$ with respect to GND.
4	7,8	GND	Ground
5	9, 10	Vout	High-Side Voltage Out
6	+	C2+	Positive terminal to secondary charge-pump capacitor.
7		C1-	Negative terminal to primary charge-pump capacitor.
8	14	Vcc	Input Supply

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#### **Output Ripple**

VOUT ripple is typically 50mV peak-to-peak with VCC = +5V, C1 and C2 =  $0.047\mu$ F, and C3 =  $1\mu$ F (*Typical Operating Characteristics*). Ripple can be reduced by increasing the ratio between the output storage capacitor C3 and C1 and C2. This is usually accomplished by increasing C3 and keeping C1 and C2 in the  $0.01\mu$ F to  $0.047\mu$ F range. For example, if C1 and C2 are  $0.047\mu$ F (VCC must not exceed 13V) and C3 is  $10\mu$ F, output ripple typically falls to 15mV (*Typical Operating Characteristics*). Similarly, MAX623 output ripple is reduced by adding an external storage capacitor from VOUT to VCC.

#### **Capacitor Selection**

Capacitor type is unimportant when selecting capacitors for the MAX622. However, when V<sub>CC</sub> exceeds 13V, C1 and C2 must be no greater than  $0.01\mu$ F. Using larger value capacitors with input voltages above 13V causes excessive amounts of energy to pass through internal

switches during charge-pump cycles. This may damage the device.

#### **Output Protection** The MAX622/MAX623 are not internally short-circuit protected. In applications where the output is suscep-

MAX622/MAX623

protected. In applications where the output is susceptible to short circuit, external output short-circuit protection must be provided. Accomplish this by connecting a resistor between VOUT and the load to limit output current to less than 25mA. The resistor value is determined by the following formula:

R<sub>CL</sub> ≥  $\frac{V_{CC}}{25mA}$ 

#### \_\_\_\_**Typical Applications** Simple Single-Load Switch

A single switch can be made with the MAX622/MAX623 and a MAX480 op amp configured as a comparator



Figure 2. MAX622/MAX623 Quiescent Supply-Current Test Circuits

(Figure 3). The switch is turned on by applying VBATT to the ON/OFF input and turned off by pulling it to GND.

#### **One MAX622 Drives** Six High-Side Switches

Multiple subsystems or modules can be turned on and off using a single MAX622 and an open-drain hex buffer such as the 74C906 (Figure 4). The drains of all buffer outputs are pulled up through resistors to the MAX622's VOUT. The pull-up resistance depends on the number of channels being used with the MAX622/MAX623 and power-dissipation limitations. The minimum pull-up resistor value is determined by the number of channels paralleled on each high-side power supply and the high-side output current from the MAX622/MAX623 at a given supply voltage, calculated as follows:

## $R_{MIN} = \frac{V_{OUT} \times (number of channels)}{V_{OUT} \times (number of channels)}$ lout

where  $V_{OUT}$  is the high-side output voltage and  $I_{OUT}$  is the output current of the MAX622.

For example, assuming an output current of 1mA and six channels, as in Figure 4, the minimum pull-up resistor value that will not excessively load the MAX622 is about  $100k\Omega$ , assuming all six channels are pulled low at the same time. The value of the pull-up resistor also affects the turn-on time of each FET, and hence the amount of

energy dissipated in the FET during turn on. The rate of rise of VGS is limited by the RC time constant of the pull-up resistor and FET gate capacitance: waste power will be dissipated in the FET equal to  $(I_{LOAD})^2 \times r_{DS}$  during the RC time period.

#### **H-Bridge Motor Driver**

An H-bridge motor driver is shown in Figure 5. The motor direction can be controlled by toggling between IN1 and IN2 of the DG303 analog switch. Each switch section turns on the appropriate FET pair which passes current through the motor in the desired direction.

#### **Battery-Load Controller**

In Figure 6, a MAX8211 undervoltage detector detects the battery's end-of-life, and a MAX622 high-side power supply turns the power FET switch on. During normal operation, the MAX8211 Hysteresis pin powers the MAX622, providing gate-drive to keep the FET off. When the battery reaches its discharge threshold (end-of-life), the MAX8211 output pulls the FET gate low, cutting off current to the load. At the same time, the Hysteresis pin goes low, turning off the MAX622. As a result, supply current is approximately 10µA in the load-disconnected condition.



# MAX622/MAX623

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(Figure 3). The switch is turned on by applying VBATT to the ON/OFF input and turned off by pulling it to GND.

#### One MAX622 Drives Six High-Side Switches

Multiple subsystems or modules can be turned on and off using a single MAX622 and an open-drain hex buffer such as the 74C906 (Figure 4). The drains of all buffer outputs are pulled up through resistors to the MAX622's VOUT. The pull-up resistance depends on the number of channels being used with the MAX622/MAX623 and power-dissipation limitations. The minimum pull-up resistor value is determined by the number of channels paralleled on each high-side power supply and the highside output current from the MAX622/MAX623 at a given supply voltage, calculated as follows:

 $R_{MIN} = \frac{V_{OUT} \times (number of channels)}{I_{OUT}}$ 

where  $V_{OUT}$  is the high-side output voltage and  $I_{OUT}$  is the output current of the MAX622.

For example, assuming an output current of 1mA and six channels, as in Figure 4, the minimum pull-up resistor value that will not excessively load the MAX622 is about 100k $\Omega$ , assuming all six channels are pulled low at the same time. The value of the pull-up resistor also affects the turn-on time of each FET, and hence the amount of

energy dissipated in the FET during turn on. The rate of rise of VGS is limited by the RC time constant of the pull-up resistor and FET gate capacitance: waste power will be dissipated in the FET equal to  $(I_{LOAD})^2 \times r_{DS}$  during the RC time period.

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An H-bridge motor driver is shown in Figure 5. The motor direction can be controlled by toggling between IN1 and IN2 of the DG303 analog switch. Each switch section turns on the appropriate FET pair which passes current through the motor in the desired direction.

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Figure 4. A Single MAX622 Drives Six High-Side Switches

#### 4-Channel Load Switch With No Pull-Up Resistors

Multiple high-side switches can be driven from a single MAX622/MAX623 high-side power supply with no pull-up resistors on the FET gates. In Figure 7, a MAX622 supplies high-side voltage to a MAX333 quad analog switch to control any one of four high-side switches. The FET gates are normally connected to ground when the MAX333 logic inputs are low.

#### Low-Dropout Regulator

In Figure 8, a MAX622 high-side power supply powers an LM10 reference and op-amp combination, providing sufficient gate drive to turn on the FET. This allows the regulator to achieve less than 70mV dropout at 1A load using an IRF541, and just under 20mV for a SMP60N06.

The 200mV reference section is configured for a gain of 25 (e.g.  $200mV \times 25 = 5V$ ) and connects to the noninverting input of the op amp; the regulator's output connects directly to the inverting input. The op amp amplifies the error between its inputs and varies the gate drive to the FET, regulating the output. Capacitor C6 reduces transients due to load changes; its size depends on the

magnitude of the load change in the application and can be reduced or eliminated if the load remains relatively constant. With C6 =  $1000\mu$ F, the output transient to a 1A load pulsed at 20Hz is typically less than 150mV. The regulator is turned on by applying VBATT to the Enable/Shutdown input and turned off by pulling this input to ground.

The regulator output voltage. VouT. is set by the ratio of R1 to R2, calculated as follows:

$$R2 = R1 \left( \frac{V_{O}UT}{0.2} - 1 \right)$$

If the application does not require logic shutdown, connect the MAX622 VCC pin directly to the battery and eliminate D2.





Figure 6. Battery-Load Controller Prevents Excessive Load at Battery End-of-Life

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**NOTE:** Connect substrate to VOUT. MAX622/MAX623 Transistor Count: 158

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