Order Number: MPC9331/D Rev 4, 02/2003

3.3V 1:6 LVCMOS PLL Clock Generator

The MPC9331 is a 3.3V compatible, 1:6 PLL based clock generator targeted for high performance low-skew clock distribution in mid-range to high-performance telecom, networking, and computing applications. With output frequencies up to 240 MHz and output skews less than 150 ps, the device meets the needs of most the demanding clock applications. The MPC9331 is specified for the temperature range of 0° C to $+70^{\circ}$ C.

Features

- 1:6 PLL based low-voltage clock generator
- · 3.3V power supply
- Generates clock signals up to 240 MHz
- Maximum output skew of 150 ps
- Differential LVPECL reference clock input
- Alternative LVCMOS PLL reference clock input
- Internal and external PLL feedback
- Supports zero-delay operation in external feedback mode
- PLL multiplies the reference clock by 4x, 3x, 2x, 1x, 4/3x, 3/2x, 2/3x, x/2, x/3 or x/4
- Synchronous output clock stop in logic low eliminates output runt pulses
- Power_down feature reduces output clock frequency
- · Drives up to 12 clock lines
- 32 lead LQFP packaging
- Ambient temperature range 0°C to +70°C
- Internal Power–Up Reset
- Pin and function compatible to the MPC931

Functional Description

The MPC9331 utilizes PLL technology to frequency lock its outputs onto an input reference clock. Normal operation of the MPC9331 requires either the selection of internal PLL feedback or the connection of one of the device outputs to the feedback input to close the PLL feedback path in external feedback mode. The reference clock frequency and the divider for the feedback path determine the VCO frequency. Both must be selected to match the VCO frequency range. In external PLL feedback configuration and with the available post-PLL dividers (divide-by-2, divide-by-4, and divide-by-6), the internal VCO of the MPC9331 is running at either 2x, 4x, 6x, 8x, or 12x of the reference clock frequency. In internal feedback configuration (divide-by-8) the internal VCO is running 8x of the reference frequency. The frequency of the QA, QB, QC output banks is a division of the VCO frequency and can be configured independently for each output bank using the FSELA, FSELB, and FSELC pins, respectively. The available output to input frequency ratios are 4x, 3x, 2x, 1x, 4/3x, 3/2x, 2/3x, x/2, x/3, or x/4.

The REF_SEL pin selects the differential LVPECL or the LVCMOS compatible input as the reference clock signal. The PLL_EN control selects the PLL bypass configuration for test and diagnosis. In this configuration, the selected input reference clock is routed directly to the output dividers bypassing the PLL. The PLL bypass is fully static and the minimum clock frequency specification and all other PLL characteristics do not apply. The outputs can be disabled (high-impedance) by deasserting the OE/MR pin. In the PLL configuration with external feedback selected, deasserting OE/MR causes the PLL to loose lock due to missing feedback signal presence at FB_IN. Asserting OE/MR will enable the outputs and close the phase locked loop, enabling the PLL to recover to normal operation. The MPC9331 output clock stop control allows the outputs to start and stop synchronously in logic low state, without the potential generation of runt pulses.

The MPC9331 is fully 3.3V compatible and requires no external loop filter components. The inputs (except PCLK) accept LVCMOS except signals while the outputs provide LVCMOS compatible levels with the capability to drive terminated 50 Ω transmission lines. For series terminated transmission lines, each of the MPC9331 outputs can drive one or two traces giving the devices an effective fanout of 1:12. The device is packaged in a 7x7 mm² 32-lead LQFP package.

MPC9331

LOW VOLTAGE 3.3V LVCMOS 1:6 CLOCK GENERATOR



FA SUFFIX 32 LEAD LQFP PACKAGE CASE 873A





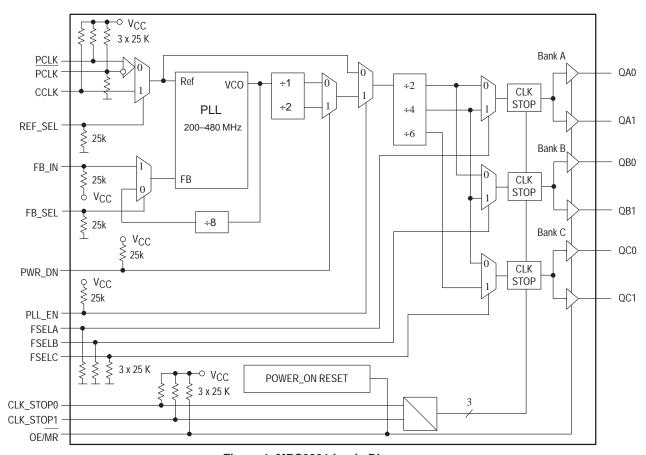
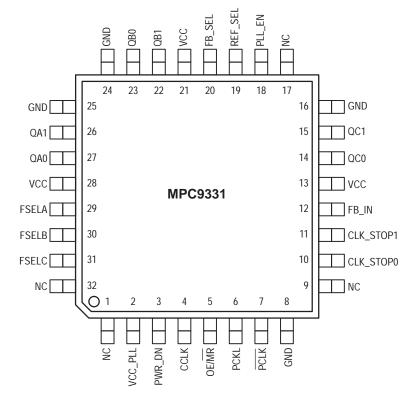


Figure 1. MPC9331 Logic Diagram



It is recommended to use an external RC filter for the analog VCC_PLL power supply pin. Please see application section for details.

Figure 2. MPC9331 32-Lead Package Pinout (Top View)

Table 1. Pin Configuration

Pin	I/O	Туре	Function
CCLK	Input	LVCMOS	PLL reference clock signal
PCLK, PCLK	Input	LVPECL	Differential PECL reference clock signal
FB_IN	Input	LVCMOS	PLL feedback signal input, connect to an output
FB_SEL	Input	LVCMOS	Feedback select
REF_SEL	Input	LVCMOS	Reference clock select
PWR_DN	Input	LVCMOS	Output frequency and power down select
FSELA	Input	LVCMOS	Frequency divider select for bank A outputs
FSELB	Input	LVCMOS	Frequency divider select for bank B outputs
FSELC	Input	LVCMOS	Frequency divider select for bank C outputs
PLL_EN	Input	LVCMOS	PLL enable/disable
CLK_STOP0-1	Input	LVCMOS	Clock output enable/disable
OE/MR	Input	LVCMOS	Output enable/disable (high-impedance tristate) and device reset
QA0-1, QB0-1, QC0-1	Output	LVCMOS	Clock outputs
GND	Supply	Ground	Negative power supply (GND)
VCC_PLL	Supply	VCC	PLL positive power supply (analog power supply). It is recommended to use external RC filter for the analog power supply pin V _{CC_PLL} . Please see applications section for details.
VCC	Supply	VCC	Positive power supply for I/O and core. All V _{CC} pins must be connected to the positive power supply for correct operation

Table 2. Function Table

Control	Default	0	1
REF_SEL	0	PCLK is the PLL reference clock	CCLK is the PLL reference clock
FB_SEL	1	Internal PLL feedback of 8. f _{VCO} = 8 * f _{ref}	External feedback. Zero-delay operation enabled for CCLK or PCLK as reference clock
PLL_EN	1	Test mode with PLL disabled. The reference clock is substituted for the internal VCO output. MPC9331 is fully static and no minimum frequency limit applies. All PLL related AC characteristics are not applicable.	Normal operation mode with PLL enabled.
PWR_DN	1	VCO ÷ 1 (High output frequency range)	VCO ÷ 2 (Low output frequency range)
FSELA	0	Output divider ÷ 2	Output divider ÷ 4
FSELB	0	Output divider ÷ 2	Output divider ÷ 4
FSELC	0	Output divider ÷ 4	Output divider ÷ 6
OE/MR	1	Outputs disabled (high-impedance state) and reset of the device. During reset in external feedback configuration, the PLL feedback loop is open. The VCO is tied to its lowest frequency. The MPC9331 requires reset after any loss of PLL lock. Loss of PLL lock may occur when the external feedback path is interrupted. The length of the reset pulse should be greater than one reference clock cycle (CCLK or PCLK). Reset does not affect PLL lock in internal feedback configuration.	Outputs enabled (active)
CLK_STOP[0:1]	11	See Table 3	

PWR_DN, FSELA, FSELB and FSELC control the operating PLL frequency range and input/output frequency ratios. See Tables 8 – 10 for supported frequency ranges and output to input frequency ratios.

Table 3. Clock Output Synchronous Disable (CLK_STOP) Function Table ^a

CLK_STOP0	CLK_STOP1	QA[0:1]	QB[0:1]	QC[0:1]
0	0	Active	Stopped in logic L state	Stopped in logic L state
0	1	Active	Stopped in logic L state	Active
1	0	Stopped in logic L state	Stopped in logic L state	Active
1	1	Active	Active	Active

a. Output operation for OE/MR=1 (outputs enabled). OE/MR=0 will high-impedance tristate all outputs independend on CLK_STOP[0:1]

Table 4. General Specifications

Symbol	Characteristics	Min	Тур	Max	Unit	Condition
VTT	Output termination voltage		V _{CC} ÷ 2		V	
MM	ESD protection (Machine model)	200			V	
HBM	ESD protection (Human body model)	2000			V	
LU	Latch-up immunity	200			mA	
C _{PD}	Power dissipation capacitance		10		pF	Per output
CIN	Input capacitance		4.0		pF	Inputs

Table 5. Absolute Maximum Ratings^a

Symbol	Characteristics	Min	Max	Unit	Condition
Vcc	Supply Voltage	-0.3	3.9	٧	
V _{IN}	DC Input Voltage	-0.3	V _{CC} + 0.3	٧	
Vout	DC Output Voltage	-0.3	V _{CC} + 0.3	V	
IIN	DC Input Current		±20	mA	
lout	DC Output Current		±50	mA	
TS	Storage temperature	-65	125	°C	

a Absolute maximum continuos ratings are those maximum values beyond which damage to the device may occur. Exposure to these conditions or conditions beyond those indicated may adversely affect device reliability. Functional operation at absolute-maximum-rated conditions is not implied.

Table 6. DC Characteristics (V $_{CC}$ = 3.3V \pm 5%, T $_{A}$ = 0°C to +70°C)

Symbol	Characteristics	Min	Тур	Max	Unit	Condition
VIH	Input high voltage	2.0		V _{CC} + 0.3	V	LVCMOS
VIL	Input low voltage			0.8	V	LVCMOS
VPP	Peak-to-peak input voltage PCLK, PCLK	250			mV	LVPECL
VCMR ^a	Common Mode Range PCLK, PCLK	1.0		V _{CC} - 0.6	V	LVPECL
Voн	Output High Voltage	2.4			V	I _{OH} = -24 mA ^b
VOL	Output Low Voltage			0.55 0.30	V V	I _{OL} = 24 mA I _{OL} = 12 mA
ZOUT	Output impedance		14 - 17		Ω	
I _{IN}	Input Current ^C			±200	μΑ	V _{IN} = V _{CC} or GND
ICC_PLL	Maximum PLL Supply Current		8.0	12	mA	VCC_PLL Pin
Iccq	Maximum Quiescent Supply Current ^d			26	mA	All V _{CC} Pins

a V_{CMR} (DC) is the crosspoint of the differential input signal. Functional operation is obtained when the crosspoint is within the V_{CMR} range and the input swing lies within the V_{PP} (DC) specification

b The MPC9331 is capable of driving 50Ω transmission lines on the incident edge. Each output drives one 50Ω parallel terminated transmission line to a termination voltage of V_{TT}. Alternatively, the device drives up to two 50Ω series terminated transmission lines.

c Inputs have pull-down or pull-up resistors affecting the input current.

d OE/MR=0 (outputs in high–impedance state).

Table 7. AC Characteristics $(V_{CC} = 3.3V \pm 5\%, T_A = 0^{\circ}C \text{ to } +70^{\circ}C)^2$

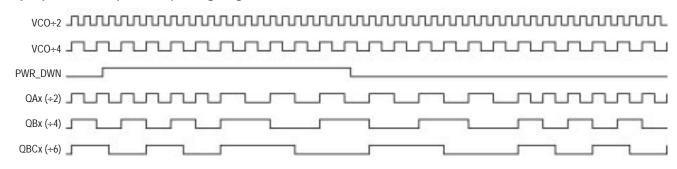
Symbol	Characteristics	Min	Тур	Max	Unit	Condition
^f REF	Input reference frequency PLL mode, external feedback +4 feedback +6 feedback +8 feedback +12 feedback PLL mode, internal feedback Input reference frequency in PLL bypass modeb	100.0 50.0 33.3 25.0 16.67 25.0		240.0 120.0 80.0 60.0 40.0 60.0 240	MHz MHz MHz MHz MHz MHz MHz	PLL locked
fvco	VCO lock frequency range ^C	200		480	MHz	
fMAX	Output Frequency ÷2 output ÷4 output ÷6 output ÷8 output ÷12 output	100.0 50.0 33.3 25.0 16.67		240.0 120.0 80.0 60.0 40.0	MHz MHz MHz MHz MHz	PLL locked
VPP	Peak-to-peak input voltage PCLK, PCLK	400		1000	mV	LVPECL
VCMR ^d	Common Mode Range PCLK, PCLK	1.2		V _{CC} - 0.9	V	LVPECL
t _{PW,MIN}	Input Reference Pulse Width ^e	2.0			ns	
tR, tF	CCLK Input Rise/Fall Time ^f			1.0	ns	0.8 to 2.0V
t _(∅)	Propagation Delay (static phase offset) CCLK to FB_IN9 CCLK to FB_IN9	-250 -180 -3.0	-130 -30	-50 +120 +3.0	ps ps °	FB_SEL = 1 and PLL locked
tsk(O)	Output-to-output Skew			150	ps	
DC	Output duty cycle ⁱ	(T ÷ 2)–500	T÷2	(T÷2)+500	ps	
t _R , t _F	Output Rise/Fall Time	0.1		1.0	ns	0.55 to 2.4V
^t PLZ, HZ	Output Disable Time			8.0	ns	
^t PZL, LZ	Output Enable Time			10	ns	
^t JIT(CC)	Cycle-to-cycle jitterİ			200	ps	
^t JIT(PER)	Period Jitter ^j			125	ps	
^t JIT(∅)	I/O Phase Jitter RMS (1 σ)			25	ps	
BW	PLL closed loop bandwidth ^k ÷ 4 feedback PLL mode, external feedback ÷ 6 feedback ÷ 8 feedback ÷ 12 feedback		2.0-8.0 1.2-4.0 1.0-3.0 0.7-2.0		MHz MHz MHz MHz	
tLOCK	Maximum PLL Lock Time			10	ms	

NOTES:

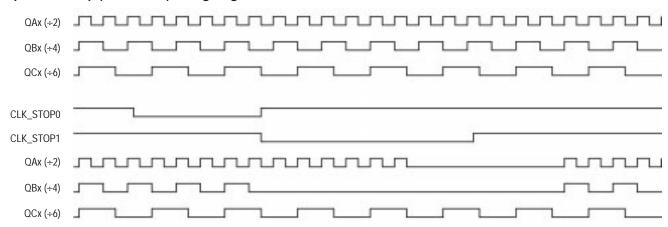
- AC characteristics apply for parallel output termination of 50Ω to VTT.
- In bypass mode, the MPC9331 divides the input reference clock.
- The input frequency f_{REF} must match the VCO frequency range divided by the feedback divider ratio FB: f_{REF} = f_{VCO} ÷ FB.
- V_{CMR} (AC) is the crosspoint of the differential input signal. Normal AC operation is obtained when the crosspoint is within the V_{CMR} range and the input swing lies within the Vpp (AC) specification. Violation of VCMR or Vpp impacts static phase offset t(Ø).
- Calculation of reference duty cycle limits: DCREF,MIN = $t_{PW,MIN} \cdot f_{REF} \cdot 100\%$ and DCREF,MAX = $t_{REF,MIN} \cdot f_{REF,MIN} \cdot f_{REF,MIN} \cdot f_{REF,MIN} = t_{PW,MIN} \cdot f_{REF,MIN} \cdot f_{REF,MIN} = t_{PW,MIN} \cdot f_{REF,MIN} = t_{PW,MIN$ be guaranteed if tR, tF are within the specified range.
- Data valid for fREF=50 MHz and a PLL feedback of +8 (e.g. QAx connected to FB_IN and FSELA=1, PWR_DN=1).
- Data valid for 16.67 MHz < f_{REF} < 100 MHz and any feedback divider. $t_{Sk(O)}[s] = t_{Sk(O)}[^{\circ}] \div (f_{REF} \cdot 360^{\circ})$.
- Output duty cycle is DC = $(0.5 \pm 500 \text{ ps} \cdot f_{OUT}) \cdot 100\%$. (e.g. the DC range at $f_{OUT} = 100 \text{ MHz}$ is 45% < DC < 55%).
- All outputs in ÷4 divider configuration.
- -3 dB point of PLL transfer characteristics.

APPLICATIONS INFORMATION

Output power down (PWR_DN) timing diagram



Output clock stop (CLK_STOP) timing diagram



Programming the MPC9331

The MPC9331 supports output clock frequencies from 16.67 to 240 MHz. Different feedback and output divider configurations can be used to achieve the desired input to output frequency relationship. The feedback frequency and divider should be used to situate the VCO in the frequency lock range between 200 and 480 MHz for stable and optimal

operation. The FSELA, FSELB, FSELC and PWR_DN pins select the desired output clock frequencies. Possible frequency ratios of the reference clock input to the outputs are 4:1, 3:1, 2:1, 1:1, 1:2, 2:3 and 3:2. Table 8 illustrates the various output configurations and frequency ratios supported by the MPC9331. See also Table 8 and 9 for further reference.

Table 8. MPC9331 Example Configurations (Internal Feedback and FB_SEL = 0)

frefa [MHz]	PWR_DN	FSELA	FSELB	FSELC	QA[0:1]:fref ratio	QB[0:1]:fref ratio	QC[0:1]:fref ratio
	0	0	0	0	fref · 4 (100-240 MHz)	fref · 4 (100-240 MHz)	fref · 2 (50-120 MHz)
	0	0	0	1	fref · 4 (100-240 MHz)	fref · 4 (100-240 MHz)	fref ·4÷3 (33.3-80 MHz)
	0	0	1	0	fref · 4 (100-240 MHz)	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)
	0	0	1	1	fref · 4 (100-240 MHz)	fref · 2 (50-120 MHz)	fref ·4÷3 (33.3-80 MHz)
	0	1	0	0	fref · 2 (50-120 MHz)	fref · 4 (100-240 MHz)	fref · 2 (50-120 MHz)
	0	1	0	1	fref · 2 (50-120 MHz)	fref · 4 (100-240 MHz)	fref ·4÷3 (33.3-80 MHz)
	0	1	1	0	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)
25.0 - 60.0	0	1	1	1	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)	fref ·4÷3 (33.3-80 MHz)
	1	0	0	0	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)	fref (25.0-60 MHz)
	1	0	0	1	fref · 2 (50-120 MHz)	fref · 2 (50-120 MHz)	fref ·2÷3 (16.67-40 MHz)
	1	0	1	0	fref · 2 (50-120 MHz)	fref (25.0-60 MHz)	fref (25.0-60 MHz)
	1	0	1	1	fref · 2 (50-120 MHz)	fref (25.0-60 MHz)	fref ·2÷3 (16.67-40 MHz)
	1	1	0	0	fref (25.0-60 MHz)	fref · 2 (50-120 MHz)	fref (25.0-60 MHz)
	1	1	0	1	fref (25.0-60 MHz)	fref · 2 (50-120 MHz)	fref ·2÷3 (16.67-40 MHz)
	1	1	1	0	fref (25.0-60 MHz)	fref (25.0-60 MHz)	fref (25.0-60 MHz)
	1	1	1	1	fref (25.0-60 MHz)	fref (25.0-60 MHz)	fref ·2÷3 (16.67-40 MHz)

a. fref is the input clock reference frequency (CCLK or PCLK)

Table 9. MPC9331 Example Configurations (External Feedback and PWR_DN = 0)

PLL Feedback	fref ^a [MHz]	FSELA	FSELB	FSELC	QA[0:1]:fref ratio	QB[0:1]:fref ratio	QC[0:1]:fref ratio
	100 - 240	0	0	0	fref (100-240 MHz)	fref (100-240 MHz)	fref ÷ 2 (50-120 MHz)
VCO ÷ 2b		0	0	1	fref (100-240 MHz)	fref (100-240 MHz)	fref ÷ 3 (33.3-80 MHz)
VOO + 2*		0	1	0	fref (100-240 MHz)	fref ÷ 2 (50-120 MHz)	fref ÷ 2 (50-120 MHz)
		0	1	1	fref (100-240 MHz)	fref ÷ 2 (50-120 MHz)	fref ÷ 3 (33.3-80 MHz)
	50 - 120	1	0	0	fref (50-120 MHz)	fref ·2 (100-240 MHz)	fref (50-120 MHz)
VCO ÷ 4 ^C		1	0	1	fref (50-120 MHz)	fref ·2 (100-240 MHz)	fref ·2÷3 (33.3-80 MHz)
VCO + 4*		1	1	0	fref (50-120 MHz)	fref (100-240 MHz)	fref (50-120 MHz)
		1	1	1	fref (50-120 MHz)	fref (100-240 MHz)	fref ·2 ÷ 3 (33.3-80 MHz)
	33.3-80	0	0	1	fref ·3 (100-240 MHz)	fref ·3 (100-240 MHz)	fref (33.3-80 MHz)
VCO ÷ 6d		0	1	1	fref ·3 (100-240 MHz)	fref ·3 ÷ 2 (50-120 MHz)	fref (33.3-80 MHz)
VCO ÷ 64		1	0	1	fref ·3 ÷ 2 (50-120 MHz)	fref ·3 (100-240 MHz)	fref (33.3-80 MHz)
		1	1	1	fref ·3 ÷ 2 (50-120 MHz)	fref ⋅3 ÷ 2 (50-120 MHz)	fref (33.3-80 MHz)

a. fref is the input clock reference frequency (CCLK or PCLK)

Table 10. MPC9331 Example Configurations (External Feedback and PWR_DN = 1)

PLL	fref ^a [MHz]	FSELA	FSELB	FSELC	QA[0:1]:fref ratio	QB[0:1]:fref ratio	QC[0:1]:fref ratio
Feedback							
	25.0 - 60.0	1	0	0	fref (25-60 MHz)	fref ·2 (50-120 MHz)	fref (2.25-60 MHz)
VCO ÷ 8b		1	0	1	fref (25-60 MHz)	fref ·2 (50-120 MHz)	fref ·2÷3 (16.6-40 MHz)
VOO . 0		1	1	0	fref (25-60 MHz)	fref (25-60 MHz)	fref (25-60 MHz)
		1	1	1	fref (25-60 MHz)	fref (25-60 MHz)	fref ·2÷3 (16.6-40 MHz)
	16.67 - 40	0	0	1	fref ·3 (50-120 MHz)	fref ·3 (50-120 MHz)	fref (16.67-40 MHz)
VCO ÷ 12 ^C		0	1	1	fref ·3 (50-120 MHz)	fref ·3 ÷ 2 (25-60 MHz)	fref (16.67-40 MHz)
V 00 + 12°		1	0	1	fref ·3 ÷ 2 (25-60 MHz)	fref ·3 (50-120 MHz)	fref (16.67-40 MHz)
		1	1	1	fref ·3 ÷ 2 (25-60 MHz)	fref ·3 ÷ 2 (25-60 MHz)	fref (16.67-40 MHz)

a. fref is the input clock reference frequency (CCLK or PCLK)

b. QAx connected to FB_IN and FSELA = 0, PWR_DN = 0

c. QAx connected to FB_IN and FSELA = 1, PWR_DN = 0

d. QCx connected to FB_IN and FSELC = 1, PWR_DN = 0

b. QAx connected to FB_IN and FSELA = 1, PWR_DN = 1

c. QCx connected to FB_IN and FSELC = 1, PWR_DN = 1

APPLICATIONS INFORMATION

Power Supply Filtering

The MPC9331 is a mixed analog/digital product. Its analog circuitry is naturally susceptible to random noise, especially if this noise is seen on the power supply pins. Random noise on the VCC_PLL power supply impacts the device characteristics, for instance I/O jitter. The MPC9331 provides separate power supplies for the output buffers (VCC) and the phase-locked loop (VCC_PLL) of the device. The purpose of this design technique is to isolate the high switching noise digital outputs from the relatively sensitive internal analog phase-locked loop. In a digital system environment where it is more difficult to minimize noise on the power supplies a second level of isolation may be required. The simple but effective form of isolation is a power supply filter on the VCC_PLL pin for the MPC9331. Figure 7 illustrates a typical power supply filter scheme. The MPC9331 frequency and phase stability is most susceptible to noise with spectral content in the 100 kHz to 20 MHz range. Therefore the filter should be designed to target this range. The key parameter that needs to be met in the final filter design is the DC voltage drop across the series filter resistor RF. From the data sheet the I_{CC}_PLL current (the current sourced through the VCC_PLL pin) is typically 8 mA (12 mA maximum), assuming that a minimum of 3.0V must be maintained on the VCC_PLL pin.

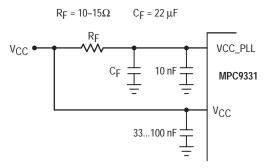


Figure 3. VCC PLL Power Supply Filter

The minimum values for RF and the filter capacitor CF are defined by the required filter characteristics: the RC filter should provide an attenuation greater than 40 dB for noise whose spectral content is above 100 kHz. In the example RC filter shown in Figure 3, the filter cut-off frequency is around 3-5 kHz and the noise attenuation at 100 kHz is better than 42 dB.

As the noise frequency crosses the series resonant point of an individual capacitor its overall impedance begins to look inductive and thus increases with increasing frequency. The parallel capacitor combination shown ensures that a low impedance path to ground exists for frequencies well above the bandwidth of the PLL. Although the MPC9331 has several design features to minimize the susceptibility to power supply noise (isolated power and grounds and fully differential PLL) there still may be applications in which overall performance is being degraded due to system power supply noise. The power supply filter schemes discussed in this section should be adequate to eliminate power supply noise related problems in most designs.

Driving Transmission Lines

The MPC9331 clock driver was designed to drive high speed signals in a terminated transmission line environment. To provide the optimum flexibility to the user the output drivers were designed to exhibit the lowest impedance possible. With an output impedance of less than 20Ω the drivers can drive either parallel or series terminated transmission lines. For more information on transmission lines the reader is referred to Motorola application note AN1091. In most high performance clock networks point-to-point distribution of signals is the method of choice. In a point-to-point scheme either series terminated or parallel terminated transmission lines can be used. The parallel technique terminates the signal at the end of the line with a 50Ω resistance to $V_{\mbox{CC}}\div2$.

This technique draws a fairly high level of DC current and thus only a single terminated line can be driven by each output of the MPC9331 clock driver. For the series terminated case however there is no DC current draw, thus the outputs can drive multiple series terminated lines. Figure 4 "Single versus Dual Transmission Lines" illustrates an output driving a single series terminated line versus two series terminated lines in parallel. When taken to its extreme the fanout of the MPC9331 clock driver is effectively doubled due to its capability to drive multiple lines.

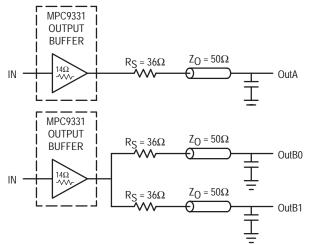


Figure 4. Single versus Dual Transmission Lines

The waveform plots in Figure 5 "Single versus Dual Line Termination Waveforms" show the simulation results of an output driving a single line versus two lines. In both cases the drive capability of the MPC9331 output buffer is more than sufficient to drive 50Ω transmission lines on the incident edge. Note from the delay measurements in the simulations a delta of only 43ps exists between the two differently loaded outputs. This suggests that the dual line driving need not be used exclusively to maintain the tight output-to-output skew of the MPC9331. The output waveform in Figure 5 "Single versus Dual Line Termination Waveforms" shows a step in the waveform, this step is caused by the impedance mismatch seen looking into the driver. The parallel combination of the 36Ω series resistor plus the output

impedance does not match the parallel combination of the line impedances. The voltage wave launched down the two lines will equal:

$$\begin{array}{l} V_L = V_S \; (\; Z_0 \div (R_S + R_0 + Z_0)) \\ Z_0 = \; 50\Omega \; || \; 50\Omega \\ R_S = \; 36\Omega \; || \; 36\Omega \\ R_0 = \; 14\Omega \\ V_L = \; 3.0 \; (\; 25 \div (18 + 14 + 25)) \\ = \; 1.31V \end{array}$$

At the load end the voltage will double, due to the near unity reflection coefficient, to 2.6V. It will then increment towards the quiescent 3.0V in steps separated by one round trip delay (in this case 4.0ns).

1 Final skew data pending specification.

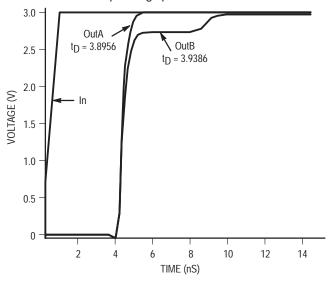


Figure 5. Single versus Dual Waveforms

Since this step is well above the threshold region it will not cause any false clock triggering, however designers may be uncomfortable with unwanted reflections on the line. To better match the impedances when driving multiple lines the situation in Figure 6 "Optimized Dual Line Termination" should be used. In this case the series terminating resistors are reduced such that when the parallel combination is added to the output buffer impedance the line impedance is perfectly matched.

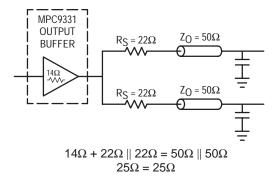


Figure 6. Optimized Dual Line Termination

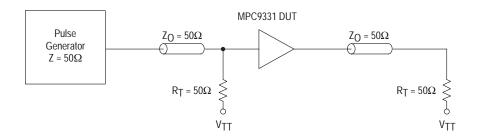
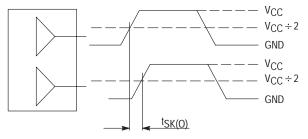
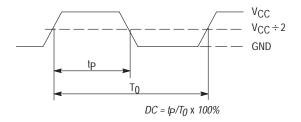


Figure 7. CCLK MPC9331 AC test reference for V_{CC} = 3.3V



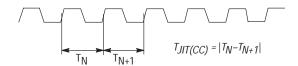
The pin-to-pin skew is defined as the worst case difference in propagation delay between any similar delay path within a single device

Figure 8. Output-to-output Skew tSK(O)



The time from the PLL controlled edge to the non controlled edge, divided by the time between PLL controlled edges, expressed as a percentage

Figure 10. Output Duty Cycle (DC)



The variation in cycle time of a signal between adjacent cycles, over a random sample of adjacent cycle pairs

Figure 12. Cycle-to-cycle Jitter

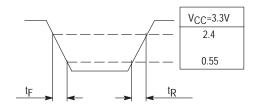


Figure 14. Output Transition Time Test Reference

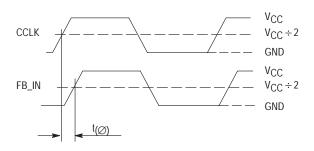
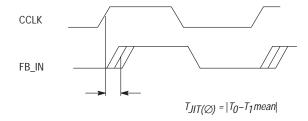
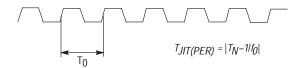


Figure 9. Propagation delay ($\mathbf{t}(\emptyset)$), static phase offset) test reference



The deviation in t_0 for a controlled edge with respect to a t_0 mean in a random sample of cycles

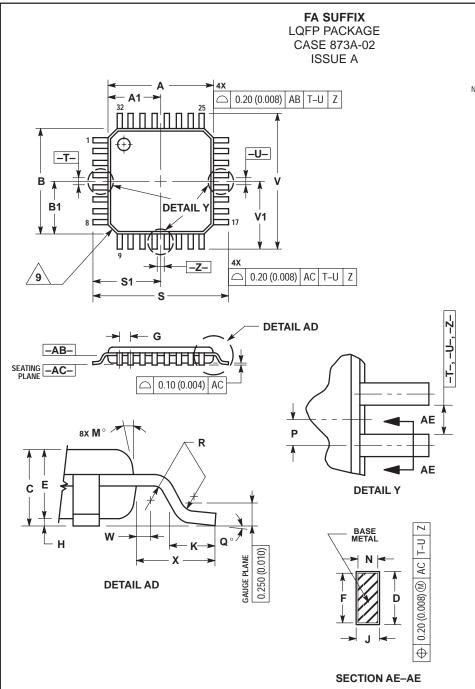
Figure 11. I/O Jitter



The deviation in cycle time of a signal with respect to the ideal period over a random sample of cycles

Figure 13. Period Jitter

OUTLINE DIMENSIONS



NOTES:

- 1 DIMENSIONING AND TOLERANCING PER ANSI
- Y14.5M, 1982. CONTROLLING DIMENSION: MILLIMETER.
- DATUM PLANE -AB- IS LOCATED AT BOTTOM
 OF LEAD AND IS COINCIDENT WITH THE LEAD WHERE THE LEAD EXITS THE PLASTIC BODY AT THE BOTTOM OF THE PARTING LINE.

 4 DATUMS -T., -U., AND -Z. TO BE DETERMINED AT DATUM PLANE -AB..

- AT DATUM PLANE AB-.

 5 DIMENSIONS S AND V TO BE DETERMINED AT SEATING PLANE AC-.

 6 DIMENSIONS A AND B DO NOT INCLUDE MOLD PROTRUSION, ALLOWABLE PROTRUSION IS 0.250 (0.010) PER SIDE. DIMENSIONS A AND B DO INCLUDE MOLD MISMATCH AND ARE
- DOT INCLUDE MOLD MISSIAN CHAND ARE
 DETERMINED AT DATUM PLANE AB-.
 7 DIMENSION D DOES NOT INCLUDE DAMBAR
 PROTRUSION. DAMBAR PROTRUSION SHALL
 NOT CAUSE THE D DIMENSION TO EXCEED 0.520 (0.020).

 8 MINIMUM SOLDER PLATE THICKNESS SHALL BE
- MINIMINION SOCIETATE THICKNESS SHALE
 0.0076 (0.0003).

 EXACT SHAPE OF EACH CORNER MAY VARY
 FROM DEPICTION.

	MILLIN	METERS	INC	HES	
DIM	MIN MAX		MIN	MAX	
Α	7.000	BSC	0.276	BSC	
A1	3.500	BSC	0.138	BSC	
В	7.000	BSC	0.276	BSC	
B1	3.500	BSC	0.138	BSC	
С	1.400	1.600	0.055	0.063	
D	0.300	0.450	0.012	0.018	
E	1.350	1.450	0.053	0.057	
F	0.300	0.400	0.012	0.016	
G	0.800	BSC	0.031 BSC		
Н	0.050	0.150	0.002	0.006	
J	0.090	0.200	0.004	0.008	
K	0.500	0.700	0.020	0.028	
M	12°	REF	12° REF		
N	0.090	0.160	0.004	0.006	
P	0.400			BSC	
Q	1°	5°	1°	5°	
R	0.150	0.250	0.006	0.010	
S	9.000	BSC	0.354	BSC	
S1	4.500	BSC	0.177 BSC		
V	9.000	BSC	0.354 BSC		
V1	4.500	BSC	0.177 BSC		
W	0.200	REF	0.008	REF	
Х	1.000	REF	0.039	REF	

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